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## VERY LARGE TELESCOPE

### GRAVITY Pipeline User Manual

VLT-MAN-ESO-19500-XXXX

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## 1 Introduction

This manual is a complete description of the data reduction recipes implemented for the GRAVITY pipeline, reflecting the status of the GRAVITY pipeline as of now.

The main part of the document is focused on the main feature of the pipeline useful to the science user of GRAVITY. The detailed appendixes may be more useful to ESO staff for the purpose of long term re-calibration and data quality control.

### 1.1 Reference and applicable documents

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- [1] *OIFits Explorer*. <http://www.jmmc.fr/oifitsexplorer>. 43
- [2] *QFitsView*. <http://www.mpe.mpg.de/ott/QFitsView/>. 43
- [3] ESO/SDD/DFS, <http://www.eso.org/cpl/>. *CPL home page*. 80
- [4] T. A. Pauls, J. S. Young, W. D. Cotton, and J. D. Monnier. A Data Exchange Standard for Optical (Visible/IR) Interferometry. *PASP*, 117:1255–1262, November 2005. 16, 47, 48, 49, 83
- [5] C.Sabet P.Ballester. *VLTI Data Interface Control Document*. ESO, 1.0 edition, 3 June 2002. VLT-SPE-ESO-15000-2764. 43, 46

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## 2 GRAVITY Instrument Description

The GRAVITY instrument has been developed under ESO contract by the GRAVITY consortium.

The main purpose of the instrument is to measure the angular separation between stars in the vicinity of the Galactic Center black hole, and even the position and motion of the infrared emission of the black hole itself during flares.

GRAVITY recombines the light beams collected by either the four 8.2m Unit Telescopes or the four VLTI Auxiliary Telescopes. The general principle of the instrument is to recombine the light coming from one (single field mode) or two (dual field mode) astronomical targets in two different beam combiners: the Fringe Tracker (FT) and the Science Combiner (SC). In single field mode, the light from the target is split between the FT and SC channels using a beam splitter, while in dual field mode a mirror directs the light from each target to their respective beam combiners. The FT is optimized to record fringes at very high frequency (up to 1 kHz), in order to measure and compensate in real time the atmospheric piston effect using a dedicated actuator in the instrument. As the observed targets are both within the atmospheric isoplanetic patch, the correction of the atmospheric piston by the FT stabilizes the fringes of the SC channel. This gives the possibility to integrate for up to several tens of seconds, and therefore reach a high sensitivity, even at relatively high spectral dispersion, on the SC channel.

The properties of the interference fringes are measured separately in the FT and SC beam combiners. GRAVITY measures the classical interferometric observables of any source, as the previous VLTI instruments (VINCI, MIDI, AMBER and PIONIER). The FT spectral resolution is limited to 5 spectral channels over the  $K$  band. The SC has three available spectral resolutions: low (40), medium (400) and high (4000), providing approximately 10, 200 and 1800 spectral channels over the  $K$  band.

The phases of the SC beam combiner are referenced to the FT using a metrology system that encompasses the optics of the VLTI up to the secondary mirror of the telescopes. Thanks to this link between the two beam combiners, GRAVITY provides very accurate measurements of the differential position of the fringe pattern obtained, for each baseline, between a reference star (in the FT channel) and the target star (in the SC channel). Given the VLTI FOV, the angular separation between the reference object and the science target is limited to 5 arcsec with the ATs and 2 arcsec with the UTs. Within this restricted separation, the final accuracy on the relative astrometry is expected to be of a few tens of  $\mu$ arcsec.

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## 3 Data flow overview

### 3.1 The concept of recipe

The pipeline is built over “recipes” that implement the basic steps of the reduction. The recipe input is a Set Of Files (SOF), which contains the list of files to reduce, associated with the required calibrations. Each recipe has a list of possible options. Each recipe produces one or several products. The recipes can be triggered by several mechanisms:

**gasgano** is the ESO user interface to classify, select files (= construct a SOF) and launch recipes.

**esorex** is the ESO command line tool to launch a recipe on any SOF manually written by the user.

**reflex** is the ESO environment allowing to reduce an entire directory in batch mode.

The GRAVITY consortium has also built a dedicated python script which browses the content of the current directory, classifies the files, writes the SOFs and automatically triggers the corresponding recipes via esorex.

### 3.2 The concept of SOF

A SOF is a consistent list of files to be sent to a recipe. Each file in the list shall be assigned a *DO Category*, which tells the recipe its purpose in the reduction. In the GRAVITY pipeline, the DO categories are trivially built from the DPR.TYPE, DPR.CATG and PRO.CATG keywords in the FITS header.

### 3.3 Instrument calibrations

In order to reduce interferometric observations, it is mandatory to calibrate the detectors and the combiners. These calibrations are obtained via dedicated observations of the internal source with all shutters closed, one shutter open at a time, two shutters open at a time, and all shutters open.

The recipe **gravity\_dark** creates the DARK calibration product, which contains the mean detector bias and the detector readout noise. It shall match the detector and the optical setup of the observation.

The recipe **gravity\_p2vm** creates the BAD (bad pixel), FLAT (internal transmission), P2VM (internal phase and contrast) and WAVE (wavelength map) calibration products. They shall match the optical setup of the observation for the SC and the FT, as well as the detector gain for the FT.

These products are all needed in order to reduce the interferometric observations of science target.

### 3.4 From raw data to raw visibilities

The first step is to reduce the raw interferometric observations into uncalibrated measurement of the visibilities and closure phases. This step is generally done file-per-file, that is each OBJECT exposure in the raw directory- has a corresponding files in product directory (although it is possible to reduce several files together). Note that

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this step includes the averaging over all the frames that compose a standard exposure. This step is rather long (several hours for an entire night).

The recipe is **gravity\_vis**.

The product (\*\_VIS) is an uncalibrated OIFITS file, containing the flux, the square visibilities, the complex visibilities and the closure phases for both the SC and the FT combiners.

The recipe produces an optional product, called P2VMRED, which contains many intermediate signals of the processing. It is very useful to assess the data quality. It is also possible to restart the reduction from the P2VMRED product, thus saving time for users who want to explore several values of recipe parameters.

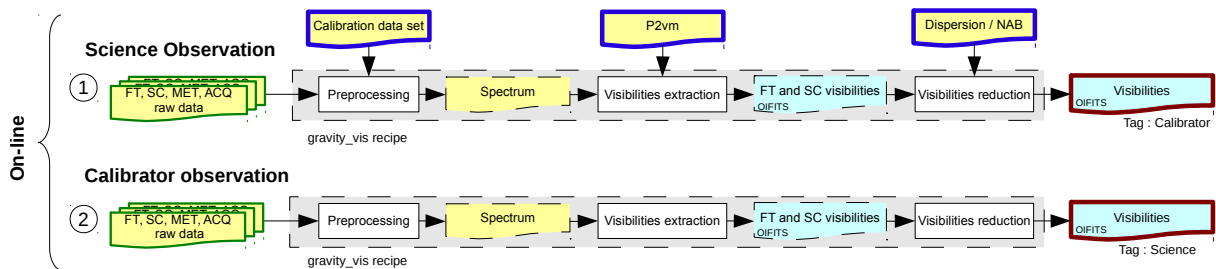


Figure 3.1: Data flow of gravity\_vis recipe.

### 3.5 From raw visibilities to calibrated visibilities

The second step is to calibrate the observation of science objects with the observation of calibration stars. This step could be performed “globally”, that is all the uncalibrated \*\_VIS oifits can be loaded first, then the pipeline searches for consistent sequences (same setup, same DIT, same wavelength table...), and then each sequence is calibrated independently with the calibration stars that could be found within it. This step is rather short (1min for an entire night).

The recipe is **gravity\_viscal**.

The product (\*\_VIS\_CALIBRATED) is a calibrated OIFITS file, ready for science.

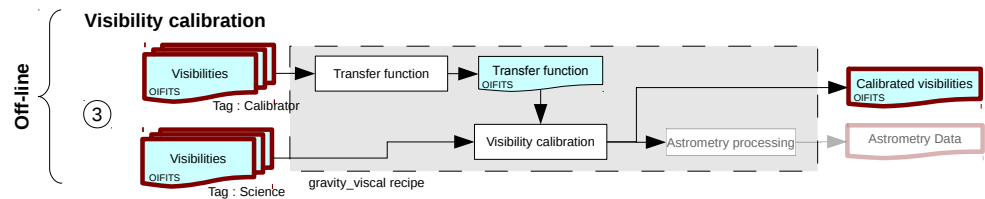


Figure 3.2: Data flow of gravity\_viscal recipe.

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## 4 Instrument Data Description

### 4.1 RAW science data

The RAW frames created when observing have the following DPR.TYPE:

<b>OBJECT,DUAL</b>	are observations of a nearby pair of objects, one feeding the fringe-tracker (FT) and the other feeding the science combiner (SC). It can be of category SCI or CAL.
<b>OBJECT,SINGLE</b>	are observations of a single object, feeding both the fringe-tracker (FT) and the science combiner (SC). It can be of category SCI or CAL.
<b>SKY,SINGLE</b> <b>SKY,DUAL</b>	are observation of an empty patch of the sky near the object in order to measure the sky brightness.

The OBJECT,DUAL and OBJECT,SINGLE types have a category DPR.CATG=SCI when observing a science target, and a category DPR.CATG=CAL when observing a calibration star used to monitor the transfer function.

### 4.2 RAW calibration data

The RAW frames used to calibrate the instrument on a daily-basis have the following DPR.TYPE:

<b>DARK</b>	are observations with all shutters closed, in order to calibrate the detector dark level and the detector + dark level noise.
<b>FLAT</b>	are observations of the internal source with one shutter open, in order to calibrate the positions of the spectra on the detectors and the internal transmission of the instrument.
<b>P2VM</b>	are observations of the internal source with two shutters open, in order to calibrate the internal contrasts and phases of the instrument.
<b>WAVE</b> <b>WAVESC</b>	are observations of the internal source with all shutters open, in order to calibrate the wavelength table, and the internal closure phases. The WAVE data are recorded by scanning on both SC and FT, with FDDL in open loop and no fringe tracking (in order to calibrate the FT wavelengths). The WAVESC data are recorded by scanning only SC, and FDDL in close-loop and fringe tracking (to calibrate the SC wavelengths).

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### 4.3 STATIC calibration

The STATIC calibration frames have the following DPR.TYPE:

<b>DISP_MODEL</b>	is the model of the optical dispersive index $n(\lambda)$ of the fiber differential delay lines (FDDL) of the instrument.
<b>DISP_VIS</b>	is an intermediate product when building DISP_MODEL, used to visualise the quality of the FDDL stretching sequence.
<b>DIAMETER_CAT</b>	is the catalog of stellar diameters used to estimate the transfer function.
<b>EOP_PARAM</b>	is a list of Earth Orientation Parameters (EOP) and DUT1 versus time. These corrections are only needed for the most demanding astrometric measurements.
<b>DIODE_POSITION</b>	contains the position of the metrology receivers

### 4.4 PRODUCT calibration data

The PRODUCT of the calibration by the recipes **gravity\_dark** and **gravity\_p2vm** are identified by the following PRO.CATG keyword:

<b>DARK</b>	contains images with the dark level and variance for the SC and FT detectors.
<b>BAD</b>	contains images with the identified bad pixels for the SC and the FT detectors.
<b>FLAT</b>	contains images of the profiles used to extract the SC spectra from the detector. There is one extracted spectrum per output of the detector and per polarisation if split (thus 24 or 48 spectra for each SC and FT combiners).
<b>WAVE</b>	contains tables with the effective wavelengths of each channel of every spectra extracted with the profile. These tables are necessary to re-align the different spectra (outputs of the detector) onto a common wavelength grid.
<b>P2VM</b>	contains tables with the internal transmission, contrast and phase of every output of the detector versus wavelength. These form the so-called pixel-2-visibility matrix used to extract the interferometric visibility from the spectra.

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## 4.5 PRODUCT science data

The products of the science reduction by the recipe **gravity\_vis** are identified by the following PRO.CATG keywords:

<b>SINGLE_SKY</b> <b>DUAL_SKY</b>	contains the mean brightness of the sky and its variance. Contrarily to DARKs, these quantities possibly depend on the instrument mode because different optics are used.
<b>SINGLE_SCI_VIS</b> <b>SINGLE_CAL_VIS</b> <b>DUAL_SCI_VIS</b> <b>DUAL_CAL_VIS</b>	are OIFITS files [4] with the uncalibrated flux, squared visibilities, complex visibilities and closure phases extracted from the raw observation of an object. SCI/CAL corresponds to a science target or a calibration star used to monitor the transfer function.
<b>SINGLE_SCI_P2VMRED</b> <b>SINGLE_CAL_P2VMRED</b> <b>DUAL_SCI_P2VMRED</b> <b>DUAL_CAL_P2VMRED</b>	are the raw data already processed through the P2VM algorithm. They contain flux per beam, and coherent flux per baseline, for each individual frame of the exposure. As such, they are intermediate products between the RAW data and the final, averaged, OIFITS. They also contain many intermediate results of the processing. The file size is huge (>200Mb). It is meant to assess the overall data quality and tune the reduction parameters. It is not used for science. Its format is inspired by OIFITS, but it is not strictly compliant.
<b>SPECTRUM</b> <b>PREPROC</b>	contains the RAW data already corrected for cosmetic and collapsed into one spectrum per combiner output. In SPECTRUM, the data are not yet re-interpolated into a common spectral wavelength grid, while this step is done in PREPROC. As such, they are debug-level intermediate products between the RAW data and the final, averaged, OIFITS.

The PRODUCT of the final calibration step by the recipe **gravity\_viscal** are identified by the following PRO.CATG keywords:

<b>SINGLE_SCI_VIS_CALIBRATED</b> <b>DUAL_SCI_VIS_CALIBRATED</b>	are the final OIFITS file of the reduction, science ready. They contain the interferometric observations calibrated with the transfer function.
<b>SINGLE_CAL_TF</b> <b>DUAL_CAL_TF</b>	are OIFITS files containing the transfer function value estimated by the corresponding observation of a calibration star. It is the observed visibility of a calibrator divided by its visibility estimated from its diameter.
<b>SINGLE_SCI_TF</b> <b>DUAL_SCI_TF</b>	are OIFITS files containing the estimated (interpolated) value of the transfer function at the time of the corresponding science target observation.



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## 5 Data Reduction

### 5.1 Graphical overview of the cascade

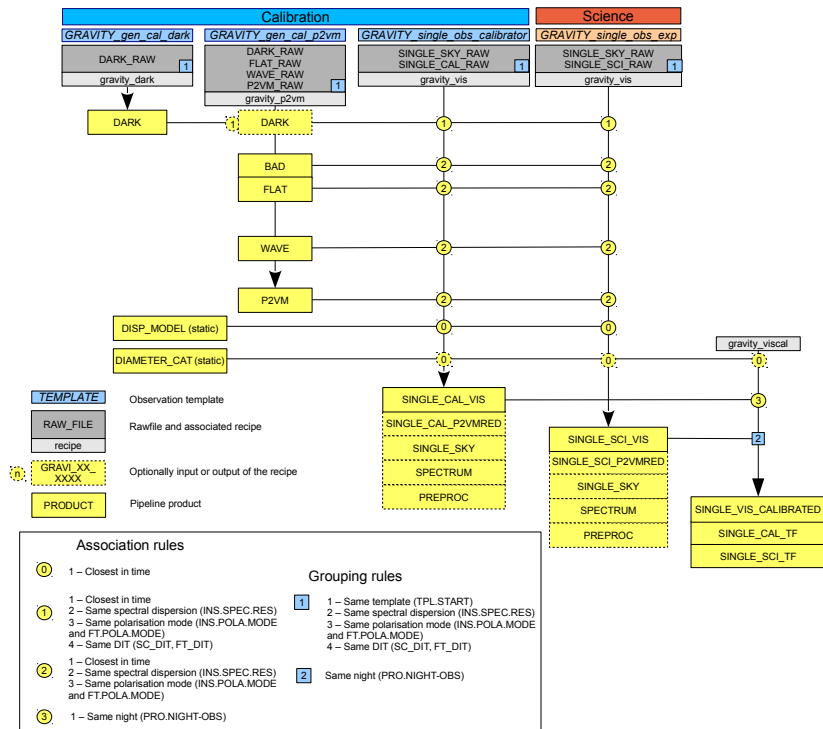


Figure 5.1: Data reduction cascade for observations in mode SINGLE. As of now, the cascade is the same for the mode DUAL.

### 5.2 Using Gasgano

*Gasgano*, provides a graphic interface for data browsing, classification and association, and offers several other utilities such as easy access to recipes documentation and preferred data display tools.

*Gasgano* can be started from the system prompt in the following way:

```
gasgano &
```

Use the *Add/Remove Files* entry of the *File* menu to load data. The data are hierarchically organised as preferred by the user. More information about a single frame can be obtained by clicking on its name.

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Frames can be selected from the main window for being processed by the appropriate recipe. Before launching the recipe, its configuration may be modified on the *Parameters* panel (on top). The window contents might be saved for later use by selecting the *Save Current Settings* entry from the *File* menu.

Please refer to the *Gasgano User's Manual* [7] for a more complete description of the *Gasgano* interface.

### 5.3 Using EsoRex

*EsoRex* is a command line utility for running pipeline recipes. It may be embedded by users into data reduction scripts for the automation of processing tasks. Users are free to define manually the input SOF and the appropriate configuration parameters.

A SOF for *EsoRex* is a simple ASCII file listing the files and their *DO Category*. Examples of SOF are given in the description of each recipe. Note that '#' is the comment character.

The basic syntax to use *EsoRex* is the following:

```
esorex [esorex_options] recipe_name [recipe_options] set_of_frames.sof
```

To get more information on how to customise *EsoRex* (see also [7]), or on a specific recipe, run the commands:

```
esorex -h
esorex -h recipe_name
esorex --man-page recipe_name
```

For more information on *EsoRex*, see <http://www.eso.org/cpl/esorex.html>.

### 5.4 Using run\_gravi\_reduce.py python script

The consortium has written a simple python script that classifies the files in the current directory, associates them with calibrations, and runs the corresponding recipes.

**Instrument calibration and data reduction** is triggered by the following script:

```
run_gravi_reduce.py [options]
```

The script performs the following steps:

1. Trigger the recipe **gravity\_dark** on all standalone DARK.
2. Trigger the recipe **gravity\_p2vm** on all sequences of 1 x DARK, 4 x FLAT, 6 x P2VM, 1 x WAVE, 1 x WAVESC.
3. Trigger the recipe **gravity\_vis** on all OBJECT,\* files.

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The script will search for (static) calibrations in the current directory if any. It will also search in the upper directory `../common_calibration/`. The products are created in the `reduced/` subdirectory.

Before triggering a recipe, the script writes the corresponding SOF and the `esorex` command in the `reduced/` subdirectory. Thus one can manually reproduce a given reduction by executing:

```
./reduced/GRAVI.XXXX_esorex.sh
```

To get more information on syntax and options, run the commands:

```
run_gravi_reduce.py -h
```

**Transfer function and trending** can be then triggered with the following script:

```
cd reduced/
run_gravi_trend.py [options]
```

The script performs the following steps:

1. Trigger the recipe **gravity\_viscal** on all `*CAL_VIS`.
2. Trigger the recipe **gravity\_viscal** on all `*SCI_VIS`.
3. Produce trending plots to check the transfer function.

The products are created in the `calibrated/` and `trend/` subdirectories.

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## 6 Known Problems

### 6.1 Spectral calibration

The spectral calibration between baselines is accurate to 0.1nm. It corresponds to half a pixel in spectral direction (thus 1/4 of the spectral resolution element) in HR.

This uncertainty can generate biases in the closure phase, which amount to  $\approx 3$ deg when observing at a group-delay of 40  $\mu$ m.

The absolute spectral calibration is accurate to 0.5nm, which corresponds to one spectral resolution elements in HR.

### 6.2 Uncertainties in products

The uncertainty of product data contains the statistical noise only, computed by bootstrapping over the NDIT samples when possible. It does not contain the calibration uncertainty.

When the number of valid DIT within an exposure is lower than 5, the statistic to compute the final error bars also include additional MonteCarlo realisation of the *theoretical* photon and detector noise (to reach 5 samples). These uncertainties are thus less realistic.

### 6.3 Metrology and polarization

The metrology snr does not follow strictly the polar. s/ polar. p brightness ratio of the beam combiners when inserting the linear polarizer and rotating the half-wave plates. The reason is that the final polarization alignment is a compromise between best possible SC/FT s/p nulling of a polarized source, and the metrology snr (= alignment between FT/SC metrology and 3rd beam). In the "detector real time display reference frame" the metrology polarization is therefore aligned with the left FT channels and the lower SC channels, that is, with the P1 polarization signals in the GRAVITY data files.

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## 7 Pipeline Recipe Interfaces

### 7.1 List of all recipes

We here list the role of each recipe. The input, output, options and QC parameters are detailed in each dedicated subsection.

gravity_badpix	Detect the bad pixels on the detectors.
gravity_biasmask	*Not Offered* Determine which pixels can be used to measure the bias of SC detector.
gravity_dark	Calibrate the detector noise and background level.
gravity_disp	Calibrate the linearity and the dispersion of the differential delay lines.
gravity_eop	Download the last values of the Earth Orientation Parameters and DUT from IERS.
gravity_image	*Not Offered* Reconstruct an image from visibilities.
gravity_nab	*Not Offered* Calibrate the narrow angle baseline.
gravity_p2vm	Detect the bad pixels on the detectors, calibrate the wavelength tables, calibrate the interferometric contrast and phase.
gravity_piezo	Calibrate the response of the piezo actuators.
gravity_postprocess	Post-process the products, to fine-tune their content.
gravity_vis	Compute the visibilities from raw observation of OBJECT.
gravity_vis_from_p2vmred	Compute the visibilities from P2VMRED intermediate product.
gravity_viscal	Calibrate visibilities with the transfer function (atmospheric interferometric response).
gravity_wavelamp	Measure the position of the Argon lines in the spectra.

### 7.2 gravity\_dark

This recipe computes the DARK calibration for the SC, the FT and the ACQ detectors. The SC detector is first debiased using the biaspixels, before computing the dark mean and rms. For detectors, the mean dark level of

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each pixel and the stdev of each pixel are saved in the output product.

1. Loop on input dark files and concatenate them
2. Compute the median and rms of these concatenated files
3. Save the product (FT, SC, ACQ camera into same product)

## Input

DO.CATG	short description
DARK_RAW	raw dark, all shutters closed (DPR.TYPE=DARK)

## Output

PRO.CATG	short description
DARK	dark calibration

## Parameters

Name	short description
–static-name –bias-method	Use static names for the products (for ESO). [FALSE] Method to average the biaspixels when cleaning-up the SC detector (only applied to MED and LOW). Ideally the same value shall be used when reducing the DARK with gravity_dark and the OBJECT with gravity_vis. <MEDIAN   MEDIAN_PER_COLUMN> [MEDIAN]

## Quality control

QC in DARK	short description
PIXBIAS AVG	Mean of the pixels used to removed the detector bias. This value shall be added to MEDIANDARK SC to trend the detector dark illumination [adu].
PIXBIAS RMS	Standard deviation over the pixels used to remove the detector bias [adu].
MEDIANDARK ACQ	Median of the dark level in the acquisition camera detector [adu]
MEDIANDARK SC	Median of the dark level in the Science Combiner detector [adu]
DARKRMS SC	Median of the dark rms (detector noise) in the Science detector [adu]

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MEANDARK FT	Mean of the dark level in the FT detector [adu]
DARKRMS FT	Median of the dark rms (detector noise) in the Fringe-Tracker detector [adu]

## Pseudo code

reference [10.1](#)

```

frameset = recipe_input_frameset
parameters = recipe_input_parameters

/* Extract DARK frameset */
dark_frameset = gravi_frameset_extract_dark_data (frameset)
nb_dark = size(dark_frameset)

/* Merge the dark frames */
for i in nb_dark :
    data = gravi_data_load_rawframe (dark_frameset[i])
    gravi_data_detector_cleanup (data, parameters) // see algo 10.1
    if i=0 :
        raw_dark = data
    else :
        gravi_data_append(raw_dark, data)

/* compute the reduced dark and save product */
dark_map = gravi_compute_dark (raw_dark) // see algo 10.2
gravi_data_save_new(dark_map, parameters)

```

## 7.3 gravity\_p2vm

This recipe reduces the internal calibrations. As a special sequence of shutter opening is required, it is advised to always build the SOF with a complete sequence of files obtained within a single execution of the p2vm calibration template. However it is still possible to input a SOF with DARK\_RAW only, or DARK\_RAW and FLAT\_RAW only. It is also possible to input a SOF with some already processed calibration (e.g WAVE).

1. Compute the dark, write product
2. Compute the flat, write product
3. Compute the badpixels, write product
4. Compute the spectral calibration, write product
5. Compute the p2vm, write product

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## Input

DO.CATG	short description
DARK_RAW	raw dark, all shutters closed (DPR.TYPE=DARK)
FLAT_RAW x4	raw flats, one shutter open (DPR.TYPE=FLAT)
P2VM_RAW x6	raw p2vms, two shutters open (DPR.TYPE=P2VM)
WAVE_RAW	raw wavelength calibration for FT (DPR.TYPE=WAVE)
WAVESC_RAW	raw wavelength calibration for SC (DPR.TYPE=WAVE,SC)

## Output

PRO.CATG	short description
DARK	dark calibration
FLAT	flat calibration
BAD	badpixel calibration
WAVE	wave calibration
P2VM	p2vm calibration

## Parameters

Name	short description
--static-name --debug-file --preproc-file --bias-method	Use static names for the products (for ESO). [FALSE] Save additional debug file(s). [FALSE] Save the PREPROC intermediate product. [FALSE] Method to average the biaspixels when cleaning-up the SC detector (only applied to MED and LOW). Ideally the same value shall be used when reducing the DARK with gravity_dark and the OBJECT with gravity_vis. <MEDIAN   MEDIAN_PER_COLUMN> [MEDIAN]
--bad-dark-threshold --profile-mode	the rms factor for dark bad pixel threshold. [10] Method to compute the extraction profile. PROFILE corresponds to the pixel intensities measured in the FLAT files (Gaussian like with FWHM of approx 1.5 pixel). This is the AUTO option for the Low and Med spectral resolution. GAUSS corresponds to a Gaussian fit of the (non-zero) pixel intensities measured in the FLAT files. BOX corresponds to a box-card of 6 pixels centered on the spectra measured in the FLAT files. This is the AUTO option for High spectral resolution. <AUTO   PROFILE   GAUSS   BOX> [AUTO]
--force-badpix-to-zero --profile-width	Force the badpixel to zero in profile. [TRUE] Width of the detector window extracted around the default position of each spectrum, and on which the profile will be applied to perform the extraction. [6]



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-interp-3pixels -force-wave-ft-equal  -wave-spectral-order -wave-mode  -phase-calibration	Interpolate with 3 pixels. [FALSE] Force the spatial order of the wavelength 2D fit for FT to zero (so all region share the same calibration). This is used to build the P2VM calibration of the TAC real-time code running on the instrument itself. [FALSE] Set the spatial order of the wavelength 2D fit for SC. [3] Define the way the wavelength are computed. PIXEL to compute the wavelength per pixels BASELINE to compute the wavelength per baseline (ABCD) AUTO to compute the wavelength per pixels in LOW, and per baseline otherwise. <PIXEL   BASELINE   AUTO> [AUTO] This option changes the phase reference of the P2VM: NONE defines phiA(lbd) at zero for all baselines (P2VM calibrates only the internal phase-shift of the beam combiner); CLOSURE defines phiA(lbd) at zero for baselines 01, 02 and 03 (P2VM calibrates the phase-shift and the closure-phase of the beam combiner); DISP defines phiA(lbd) to have zero mean and minimum GD for baselines (01,02,03); (P2VM calibrates the phase-shift, the closure-phase and the spectral-dispersion of the beam combiner); FULL defines phiA(lbd) to have zero-GD for baselines (01,02,03). <NONE   CLOSURE   DISP   FULL> [CLOSURE]
---	--

## Quality control

QC in BAD	short description
BADPIX ACQ	Total number of bad pixels on the ACQ detector
BADPIX SC	Total number of bad pixels on the SC detector
BADPIX FT	Total number of bad pixels on the FT detector
BADPIX_DARK SC/FT	Pixels with weird mean level
BADPIX_RMS SC/FT	Pixels with weird noise level
BADPIX_FLAT SC/FT	Pixels non-responding to illumination
QC in FLAT	short description
PROFILE_CENTER SC1 MED	[pixel] position of the first spectra on SC detector
PROFILE_WIDTH SC1 MED	[pixel] width of the first spectra on SC detector
PROFILE_CENTER SC13 MED	[pixel] position of the 13d spectra on SC detector
PROFILE_WIDTH SC13 MED	[pixel] width of the 13d spectra on SC detector
MEANGAIN SC	Mean gain [ADU/e] for SC detector
MEANGAIN FT	Mean gain [ADU/e] for FT detector
QC in P2VM	short description
FLUX_SCi AVG	[e/DIT/chanel/output] flux in SC (mean of files)
FLUX_FTi AVG	[e/DIT/chanel/output] flux in FT (mean of files)
P2VM_COHERENCE_AVG_SC	Average instrumental contrast of SC
P2VM_COHERENCE_AVG_FT	Average instrumental contrast of FT

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P2VM_COHERENCE_SCij	Average instrumental contrast of SC for pair ij
P2VM_COHERENCE_FTij	Average instrumental contrast of FT for pair ij
QC in WAVE	short description
REFWAVE1	Reference wavelength [m] for the below parameters
REFPOS1 SCi	Position [pix] of the REFWAVE1 in output SCi
REFPOS1 FTi	Position [pix] of the REFWAVE1 in output FTi
REFWAVE2	Reference wavelength [m] for the below parameters
REFPOS2 SCi	Position [pix] of the REFWAVE2 in output SCi
REFPOS2 FTi	Position [pix] of the REFWAVE2 in output FTi
WAVE_CORR	Model to convert the glass wavelength in vacuum wavelength
WAVE_CORR N0	Parameter of above model
WAVE_CORR N1	Parameter of above model
WAVE_CORR N2	Parameter of above model
MINWAVE SC/FT	Min wavelength [m] of SC/FT channels
MAXWAVE SC/FT	Max wavelength [m] of SC/FT channels
RMSWAVE SC/FT	Rms of residuals during polynomial wavelength fit

## Pseudo code

reference [10.1](#)

```

frameset = recipe_input_frameset
parameters = recipe_input_parameters

/* Extract DARK frameset */
dark_frameset = gravi_frameset_extract_dark_data (frameset)
darkcalib_frameset = gravi_frameset_extract_dark_map (frameset)

/* Extract FLAT frameset */
flat_frameset = gravi_frameset_extract_flat_data (frameset)
flatcalib_frameset = gravi_frameset_extract_flat_map (frameset)

/* Extract BAD frameset */
badcalib_frameset = gravi_frameset_extract_bad_map (frameset)

/* Extract WAVE frameset */
wave_frameset = gravi_frameset_extract_wave_data (frameset)
wavesc_frameset = gravi_frameset_extract_wavesc_data (frameset)
wavecalib_frameset = gravi_frameset_extract_wave_map (frameset)

/* Extract P2VM frameset */
p2vm_frameset = gravi_frameset_extract_p2vm_data (frameset)

/*(1) Compute or load the DARK file */
if (dark_frameset) then

```

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```

    data = gravi_data_load_rawframe (dark_frameset[0])
    gravi_data_detector_cleanup (data, parameters) // see algo 10.1
    dark_map = gravi_compute_dark (data) // see algo 10.2
    gravi_data_save_new(dark_map, parameters)
elseif (darkcalib_frameset) then
    dark_map = gravi_data_load_frame (darkcalib_frameset[0])

/*(2) Compute or load the BAD pixel file */
if (badcalib_frameset) then
    badpix_map = gravi_data_load_frame (badcalib_frameset[0])
elseif (dark_frameset & flat_frameset)
    for i in nb_flat_frameset
        raw_flat[i] = gravi_data_load_rawframe (flat_frameset[i])
        gravi_data_detector_cleanup (raw_flat[i], parameters)
        // see algo 10.1
    badpix_map = gravi_compute_badpix (dark_map, raw_flat)
    gravi_data_save_new (badpix_map, parameters)

/*(3) Compute or load the FLAT file */
if (flatcalib_frameset) then
    profile_map = gravi_data_load_frame (flatcalib_frameset[0]);
elseif (flat_frameset)
    for i in nb_flat_frameset
        raw_flat[i] = gravi_data_load_rawframe (flat_frameset[i])
        gravi_data_detector_cleanup (raw_flat[i], parameters)
        // see algo 10.1
    profile_map = gravi_compute_profile (raw_flat, dark_map, badpix_map,
        nb_frame_gain, parameters) // see algo 10.3
    gain = gravi_compute_gain (raw_data, nb_frame_gain, dark_map)
    cpl_propertylist_append (profile_map_header, gain)
    gravi_data_save_new (profile_map, parameters)

/*(4) Compute or load the WAVE file */
if (wavecalib_frameset) then
    wave_map = gravi_data_load_frame (wavecalib_frameset[0]);
elseif (wave_frameset)
    wave_data = gravi_data_load_rawframe_ext (wave_frameset)
    gravi_data_detector_cleanup(wave_data, parameters) // see algo 10.1
    spectrum_data = gravi_extract_spectrum (wave_sc_data, profile_map,
        dark_map, badpix_map, parameters) // see algo 10.3
    wave_map.p2vm_met = gravi_metrology_compute_p2vm (wave_data.met_table)
    gravi_wave_compute_opds (spectrum_data, wave_data.met_table)
    gravi_compute_wave (wave_map, spectrum_data, GRAVI_FT, parameters);

if (wavesc_frameset)

```

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```

    wavesc_data = gravi_data_load_rawframe_ext (wavesc_frameset)
    gravi_data_detector_cleanup(wavesc_data, parameters)
    // see algo 10.1
    spectrum_data = gravi_extract_spectrum (wavesc_data, profile_map,
        dark_map, badpix_map, parameters) // see algo 10.3
    gravi_wave_compute_opds (spectrum_data, wavesc_data.met_table)

    gravi_compute_wave (wave_map, spectrum_data, GRAVI_SC, parameters)
    gravi_data_save_new (wave_map, parameters)

/* (5) Compute the p2vm */
check(dark_map + bad_map + flat_map + wave_map)
p2vm_frameset = p2vm_frameset + wave_frameset + flat_frameset
check(size(p2vm_frameset) == 11)
p2vm_map = gravi_create_p2vm (wave_map)

for i in size(p2vm_frameset)
    data = gravi_data_load_rawframe_ext(p2vm_frameset[i])
    if (gravi_data_check_shutter (hdr_data, 1,1,1,1))
        i_wave = i
        skip_file
    gravi_data_detector_cleanup (data, parameters) // see algo 10.1
    preproc_data = gravi_extract_spectrum (data, profile_map, dark_map,
        badpix_map, parameters) // see algo 10.3
    gravi_align_spectrum(preproc_data, wave_map, p2vm_map, parameters)
    // see algo 10.5
    gravi_compute_p2vm (p2vm_map, preproc_data, valid_trans, valid_CP,
        GRAVI_DET_SC) // see algo 10.6

/* (7) P2VM normalization */
gravi_p2vm_normalisation (p2vm_map)

/* (8) Analyse the WAVE to get the phase correction
 * and the internal spectrum to latter correct */
data = gravi_data_load_rawframe_ext(p2vm_frameset[i_wave])
gravi_data_detector_cleanup (data, parameters)
preproc_data = gravi_extract_spectrum (data, profile_map, dark_map,
    badpix_map, parameters)
gravi_align_spectrum(preproc_data, wave_map, p2vm_map, parameters)
p2vmred_data = gravi_compute_p2vmred(preproc_data, p2vm_map, parameters)
if (parameters.phase-calibration == "CLOSURE")
    gravi_p2vm_phase_correction (p2vm_map, p2vmred_data, 0)
    if (parameters.phase-calibration == "DISP")
        gravi_p2vm_phase_correction (p2vm_map, p2vmred_data, 1)
    if (parameters.phase-calibration == "FULL")

```

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```
gravi_p2vm_phase_correction (p2vm_map, p2vmred_data, 2)
```

```
gravi_p2vm_transmission (p2vm_map, p2vmred_data);
```

```
gravi_data_save_new (p2vm_map, parameters)
```

## 7.4 gravity\_eop

This recipe downloads the latest version of the Earth Orientation Parameter and DUT from the IERS site. File is created in the current directory. A web connection is required.

1. Download the IERS data
2. Convert into CPL table
3. Write product

### Input

DO.CATG	short description
None	No input

### Output

PRO.CATG	short description
EOP_PARAM	EOP calibration file (gravity_eop_calib.fits)

### Parameters

Name	short description
-eop_host	FTP Host to retrieve the EOP from. [ftp.iers.org]
-eop_urlpath	FTP URL path of the EOP file to retrieve. [/products/eop/rapid/standard/finals2000A.data]

## 7.5 gravity\_vis

This recipe is associated to the observations template. Its reduces the raw data acquired on calibrator or science targets and computes the uncalibrated visibilities, saved in an OIFITS file. If several OBJECT are provided, the recipe will reduce all of them and merge the resulting data into a single OIFITS. If several SKY\_RAW are provided, the recipe reduces the first OBJECT with the first SKY file. Then each new OBJECT with the next SKY. When the number of SKYs is reached, the recipe loops back to first SKY file (so if the number of SKYs

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is larger than the number of OBJECTs, the last SKY won't be used). The recipe will reduce the data even if no SKY or no DARK is provided. However this will lead to wrong estimate of the visibility and squared visibility of the object. If the file DIAMETER\_CAT is not provided, the recipe will use the diameter provided in the header to compute the transfer function QC parameters. The tag in the DO category can be SINGLE/DUAL and CAL/SCI. They should reflect the instrument mode (SINGLE or DUAL) and the DPR.CATG of the observation (SCIENCE or CALIB). The tag in the PRO.CATG category will be SINGLE/DUAL and CAL/SCI depending on the input tag.

1. Load the input file (loop on input OBJECT files)
2. Extract the spectra (use BAD, DARK, SKY, FLAT files)
3. Interpolate the spectra into a common wavelength table (use WAVE file)
4. Compute the real-time visibilities (use P2VM file)
5. Compute additional real-time signals (SNR, GDELAY...)
6. Compute selection flags (= flag frames with SNR lower than threshold, vFactor lower than threshold...)
7. Average the real-time visibilities, considering the selection flag
8. Write the product

## Input

DO.CATG	short description
FLAT	flat calibration (PRO.CATG=FLAT)
BAD	badpixel calibration (PRO.CATG=BAD)
WAVE	wave calibration (PRO.CATG=WAVE)
P2VM	p2vm calibration (PRO.CATG=P2VM)
DARK	dark calibration (PRO.CATG=DARK)
SINGLE_SCI_RAW	raw object (DPR.TYPE=OBJECT,SINGLE)
SINGLE_SKY_RAW	raw sky (DPR.TYPE=SKY,SINGLE)
DISP_MODEL (opt)	fiber dispersion model (PRO.CATG=DISP_MODEL)
DIODE_POSITION (opt)	met receiver position (PRO.CATG=DIODE_POSITION)
DIAMETER_CAT (opt)	catalog of diameter (PRO.CATG=DIAMETER_CAT)

## Output

PRO.CATG	short description
SINGLE_SCI_VIS	OIFITS file with uncalibrated visibilities
SINGLE_SKY (opt)	sky map
SINGLE_SCI_P2VMRED (opt)	intermediate product (see detailed description of data)
SPECTRUM (opt)	intermediate product (see detailed description of data)

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PREPROC (opt)	intermediate product (see detailed description of data)
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## Parameters

Name	short description
–static-name	Use static names for the products (for ESO). [FALSE]
–bias-subtracted-file	Save the BIAS_SUBTRACTED intermediate product. [FALSE]
–spectrum-file	Save the SPECTRUM intermediate product. [FALSE]
–preproc-file	Save the PREPROC intermediate product. [FALSE]
–p2vmreduced-file	Save the P2VMRED intermediate product. [FALSE]
–astro-file	Save the ASTROREDUCED intermediate product. [FALSE]
–average-vis	Average the results from the different input files (if any) in the output product, instead of simply appending them. [FALSE]
–bias-method	Method to average the biaspixels when cleaning-up the SC detector (only applied to MED and LOW). Ideally the same value shall be used when reducing the DARK with gravity_dark and the OBJECT with gravity_vis. <MEDIAN   MEDIAN_PER_COLUMN> [MEDIAN]
–ditshift-sc	Shift the time of SC DITs by an integer value to account for lost frames in exposure (issue on the instrument side, report to instrument team). The time of all DITs in exposure are increased by ditshift x PERIOD. ditshift can be 0, positive (system has lost one SC DIT), or negative (SC desynchronized). [0]
–acq-correction-delay	Delay between the end of ACQ frame and correction offset seen by the metrology diodes, in seconds. [0.1]
–nsmooth-snr-ft	Number of samples to average coherently when computing the real-time SNR and GDELAY of the FT (shall correspond to the atmospheric coherence time). The integration window runs from -nsmooth -> +nsmooth. [5]
–snr-min-ft	SNR threshold to accept FT frames (>0). It raises the first bit (<<0) of column REJECTION_FLAG of FT. [3.0]
–global-state-min-ft	Minimum OPDC state to accept FT frames (>=0) It raises the second bit (<<1) of column REJECTION_FLAG of FT. [2.0]
–global-state-max-ft	Maximum OPDC state to accept FT frames (>=0) It raises the second bit (<<1) of column REJECTION_FLAG of FT. [4.0]
–state-min-ft	Minimum OPDC state per baseline to accept FT frames (>=0) It raises the second bit (<<1) of column REJECTION_FLAG of FT. [1.0]
–tracking-min-sc	Minimum ratio of accepted FT frames in order to accept a SC frames (0..1), that is, for each SC DIT, the fraction of the time the REJECTION_FLAG of the FT is not 0. It raises the first bit (<<0) of column REJECTION_FLAG of SC. [0.8]
–vfactor-min-sc	vFactor threshold to accept SC frame (0..1). [0.1]

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–use-met-zero	Flag to activate metrology zero calculation in OPD_DISP. If disabled all metrology zeroes are set to zero. [TRUE]
–use-tel-met	Flag to use telescope metrology in IMAGING_REF calculation. If disabled, the default, fiber coupler metrology is used instead. [FALSE]
–max-frame	Maximum number of frames to integrate coherently into an OIFITS entry. [10000]
–force-same-time	Force all baseline/quantities to have strickly the same TIME and MJD columns. [FALSE]
–debias-sc	Subtract the V2 bias from SC. [TRUE]
–debias-ft	Subtract the V2 bias from FT. [TRUE]
–nboot	Number of bootstraps to compute error (1..100). [20]
–vis-correction-sc	Correction of SC visibility from losses due to long integration, using the measured visibility losses with the FT (VFAC- TOR and/or PFACTOR) or by forcing the SC visibilities to match those of the FT (FORCE). Possible choices are: <VFAC- TOR   PFACTOR   VFAC- TOR_PFACTOR   FORCE   NONE> [VFAC- TOR]
–phase-ref-sc	Reference phase used to integrate the SC frames. Use a self- estimate of the phase, fitted by poly (SELF_REF). Use the FT phase only, interpolated in lbd (PHASE_REF). Use the FT+MET-SEP.UV phase (IMAGING_REF). <SELF_REF   PHASE_REF   IMAGING_REF   AUTO   NONE> [AUTO]
–output-phase-sc	With DIFFERENTIAL, the mean group-delay and mean phases are removed from the output VISPHI in the final OIFITS file. With ABSOLUTE, the VISPHI is kept unmodi- fied. <DIFFERENTIAL   ABSOLUTE   AUTO> [AUTO]
–flat-flux	Normalize the flux (stored in OI_FLUX binary extension) with instrument transmission recorded in the nput P2VM cal- ibration map. Consequently, the flux quantity is either the intensity level recorded n the detector, thus including the in- strument transmission (FALSE); or the intensity level at the instrument entrance (TRUE). [FALSE]
–average-sky	Average the SKYs into a master SKY. If FALSE, the recipe loops over the SKY to reduce each OBJECT with a different SKY. [FALSE]
–reduce-acq-cam	If TRUE, reduced ACQ_CAM images. [FALSE]
–reduce-acq-cam-strehl	If TRUE, add Strehl computation to ACQ_CAM processing. [FALSE]
–color-wave-correction	If TRUE, creates a new OI_WAVELENGTH_EFF with cor- rected wavelength. [FALSE]

## Quality control

QC in VIS	short description
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CHECK FLAGS	Number of messages about data integrity
CHECK MSGi	Message about data integrity
TRANS PROFILE SC	[e/e] numerical transmission at profile extraction
TRANS INTERP SC	[e/e] numerical transmission at interpolation
TRANS P2VM SC	[e/e] numerical transmission at P2VM extraction
PHASE_FTij RMS	[rad] phase residuals when tracking
TRACKING_RATIO_FTij	[%] ratio of tracking time
ACCEPTED_RATIO_FTij	[%] fraction of accepted FT frame in the final averaging
ACEEPTED_RATIO_SCij	[%] fraction of accepted SC frame in the final averaging
TAU0 OPDCij	[s] tau0 for variance of 1 rad <sup>2</sup> , computed from the fringe-tracking command to the piezo actuator.
VFACTORij_P1 AVG	mean v-factor for polar 1
VISAMP_SCij_P1 AVG	[deg] mean VISAMP for Science Combiner for polar 1
...	see all parameters
GD_SCij_P1 AVG	[m] Mean Group-Delay on Science Combiner
FLUX_FTi_P1 AVG	[e/total_int_time] mean flux over channels for Fringe Tracker
FLUXRATE_FTi_P1 SUM	[e/s] sum over channels for Fringe Tracker

If the observation is of type CALIB, and if the DIAMETER\_CAT was provided, the recipe also computes the following QC:

QC in VIS	short description
TF TRANS_FTij	Total transmission of FT
TF TRANS_SCij	Total transmission of SC
TF VISMED_SCij RELERR	TF relative error from diameter error
TF VISAMP_SCij_P1 MED	TF median over channels
TF VIS2_SCij_P1 MED	TF median over channels

## 7.6 gravity\_vis\_from\_p2vmred

This recipe averages the real-time data of P2VMRED files into a VIS product. It allows to run the reduction with different parameters (for instance for SNR thresholding) without having to re-reduce the files from scratch. Typically the reduction is 4x faster when started from this intermediate product. The tag in the DO category can be SINGLE/DUAL and CAL/SCI. They should reflect the mode (SINGLE or DUAL) and the DPR.CATG of the observation (SCIENCE or CALIB). The tag in the PRO.CATG category will be SINGLE/DUAL and CAL/SCI depending on the input tag.

1. Load the input file (loop on input files)
2. Update the selection flag
3. Average the real-time visibilities
4. Write the product

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## Input

DO.CATG	short description
SINGLE_SCI_P2VMRED	Input intermediate product

## Output

PRO.CATG	short description
SINGLE_SCI_VIS	OIFITS with uncalibrated visibilities

## Parameters

Name	short description
–static-name	Use static names for the products (for ESO). [FALSE]
–average-vis	Average the results from the different input files (if any) in the output product, instead of simply appending them. [FALSE]
–nsmooth-snr-ft	Number of samples to average coherently when computing the real-time SNR and GDELAY of the FT (shall correspond to the atmospheric coherence time). The integration window runs from -nsmooth -> +nsmooth. [5]
–snr-min-ft	SNR threshold to accept FT frames (>0). It raises the first bit (<<0) of column REJECTION_FLAG of FT. [3.0]
–global-state-min-ft	Minimum OPDC state to accept FT frames (>=0) It raises the second bit (<<1) of column REJECTION_FLAG of FT. [2.0]
–global-state-max-ft	Maximum OPDC state to accept FT frames (>=0) It raises the second bit (<<1) of column REJECTION_FLAG of FT. [4.0]
–state-min-ft	Minimum OPDC state per baseline to accept FT frames (>=0) It raises the second bit (<<1) of column REJECTION_FLAG of FT. [1.0]
–tracking-min-sc	Minimum ratio of accepted FT frames in order to accept a SC frames (0..1), that is, for each SC DIT, the fraction of the time the REJECTION_FLAG of the FT is not 0. It raises the first bit (<<0) of column REJECTION_FLAG of SC. [0.8]
–vfactor-min-sc	vFactor threshold to accept SC frame (0..1). [0.1]
–use-met-zero	Flag to activate metrology zero calculation in OPD_DISP. If disabled all metrology zeroes are set to zero. [TRUE]
–use-tel-met	Flag to use telescope metrology in IMAGING_REF calculation. If disabled, the default, fiber coupler metrology is used instead. [FALSE]
–max-frame	Maximum number of frames to integrate coherently into an OIFITS entry. [10000]
–force-same-time	Force all baseline/quantities to have strickly the same TIME and MJD columns. [FALSE]

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–debias-sc	Subtract the V2 bias from SC. [TRUE]
–debias-ft	Subtract the V2 bias from FT. [TRUE]
–nboot	Number of bootstraps to compute error (1..100). [20]
–vis-correction-sc	Correction of SC visibility from losses due to long integration, using the measured visibility losses with the FT (VFAC-TOR and/or PFACTOR) or by forcing the SC visibilities to match those of the FT (FORCE). Possible choices are: <VFAC-TOR   PFACTOR   VFAC-TOR_PFACTOR   FORCE   NONE> [VFAC-TOR]
–phase-ref-sc	Reference phase used to integrate the SC frames. Use a self-estimate of the phase, fitted by poly. (SELF_REF) Use the FT phase only, interpolated in lbd (PHASE_REF) Use the FT+MET-SEP.UV phase (IMAGING_REF). <SELF_REF   PHASE_REF   IMAGING_REF   AUTO   NONE> [AUTO]
–output-phase-sc	With DIFFERENTIAL, the mean group-delay and mean phases are removed from the output VISPHI in the final OIFITS file. With ABSOLUTE, the VISPHI is kept unmodified. <DIFFERENTIAL   ABSOLUTE   AUTO> [AUTO]
–use-existing-rejection	Use existing rejection flags (ignore related options). [FALSE]

## 7.7 gravity\_viscal

This recipe calibrates the visibilities acquired on science target using visibilities acquired on a calibrator target. If the DIAMETER\_CAT is not provided, the recipe will use the diameter provided in the header to compute the transfer function QC parameters. The corresponding keywords are INS.SOBJ.DIAMETER and FT.ROBJ.DIAMETER. The OI\_FLUX data are not yet calibrated. The tag in the DO category can be SINGLE/DUAL and CAL/SCI. The tag in the PRO.CATG category will be SINGLE/DUAL and CAL/SCI depending on the input tag.

1. Loop on all input CALIB files, compute the TF for each of them and write the corresponding product
2. Loop on all input SCIENCE files, interpolate the TF at that time, calibrate, and write the corresponding product

### Input

DO.CATG	short description
SINGLE_SCI_VIS (>=1)	visibilities on sciences
SINGLE_CAL_VIS (>=1)	visibilities on calibrators
DIAMETER_CAT (opt)	catalog of stellar diameters

### Output

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PRO.CATG	short description
SINGLE_SCI_VIS_CALIBRATED	calibrated science visibilities
SINGLE_CAL_TF	Transfer Function (TF) estimated on calibrators
SINGLE_SCI_TF	TF interpolated at the time of sciences

## Parameters

Name	short description
–static-name	Use static names for the products (for ESO). [FALSE]
–delta-time-calib [3.6e+03]	Delta time to interpolate the TF [s]
–force-calib	Force the calibration, don't check setup. [FALSE]
–nsmooth-tfvis-sc	Smooth the TF spectrally by this number of spectral bin, to enhance SNR (only apply to VIS2, VISPHI, VISAMP, T3PHI, T3AMP). This parameter is ignored in spectral mode LOW. [0]
–nsmooth-tfflux-sc	Smooth the TF spectrally by this number of spectral bin, to enhance SNR (only apply to FLUX, RVIS, IVIS). This parameter is ignored in spectral mode LOW. [0]
–maxdeg-tfvis-sc	Fit the TF spectrally by a polynomial to enhance SNR (only apply to VIS2, VISPHI, VISAMP, T3PHI, T3AMP). This parameter is ignored in spectral mode LOW. [5]
–calib-flux	Normalize the FLUX by the calibrator. [FALSE]

## 7.8 gravity\_postprocess

This recipe allows to manipulate the product of the GRAVITY pipeline, mostly the VIS. It permits to merge several files together into a single VIS file with all observations; to average the observations of one or several VIS file to increase the SNR; to remove some data (FT, SC); and to resample the SC observation with spectral binning. The list of input files can be P2VMRED, VIS, VIS\_CALIBRATED (or even RAW for some parameters). However they should all be compatible in term of setup and observed objects !! Note that the recipe performs only little checks of the input file content and structure. Thus the user shall ensure the input files are conformable (same polarisation and spectral mode for instance)

1. Load the files
2. Execute request from user
3. Write product

## Input

DO.CATG	short description
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Input files	see above
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## Output

PRO.CATG	short description
POSTPROCESSED	Output file

## Parameters

Name	short description
–average-vis	Average the results from the different input files (if any) in the output product, instead of simply appending them. [FALSE]
–fluxerr-sc	Force the uncertainty in FLUX of SC. [0.0]
–visamperr-sc	Force the uncertainty in VISAMP of SC. [0.0]
–visphierr-sc	Force the uncertainty in VISPHI of SC. [0.0]
–vis2err-sc	Force the uncertainty in VIS2 of SC. [0.0]
–force-merge	Force merging even if inconsistent data. [FALSE]
–remove-ft	Remove FT extensions. [FALSE]
–remove-sc	Remove SC extensions. [FALSE]
–remove-opdc	Remove OPDC extensions. [FALSE]
–remove-met	Remove METROLOGY related extensions. [FALSE]
–nbin-lambda-sc	Bin SC extensions in spectral dimension. [0]

## 7.9 gravity\_wavelamp

This recipe is associated to the template gravity\_wavelamp. It reduces the raw file obtained with the Argon lamp (WAVELAMP) and process it so that it can be used to calibrate the fiber dispersion (recipe gravity\_disp).

1. Extract the spectra of the Argon exposure
2. Interpolate the spectra into a common wavelength table
3. Measure the wavelength position of known Argon lines
4. Write the product

## Input

DO.CATG	short description
FLAT	flat calibration (PRO.CATG=FLAT)
BAD	badpixel calibration (PRO.CATG=BAD)
WAVE	wave calibration (PRO.CATG=WAVE)

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P2VM	p2vm calibration (PRO.CATG=P2VM)
WAVELAMP_RAW	long exposure of Argon lamp
DARK_RAW	dark of Argon exposure

## Output

PRO.CATG	short description
WAVELAMP	spectrum of Argon, with position of lines

## Parameters

Name	short description
–static-name	Use static names for the products (for ESO). [FALSE]

## 7.10 gravity\_disp

This recipe is associated to the template GRAVI\_all\_disp. It measures the phases obtained on the internal source at the position of the Argon lines and various positions (= fiber stretch) of the Fibered Differential Delay Lines (FDDL). It deduces the linearity model and the dispersion model of the differential delay lines. These models are stored as polynomials versus wavelength.

1. Reduce all the input DISP files (see gravity\_vis), write each product
2. Compute the dispersion parameters from this entire dataset
3. Write product

## Input

DO.CATG	short description
FLAT	flat calibration (PRO.CATG=FLAT)
BAD	badpixel calibration (PRO.CATG=BAD)
WAVE	wave calibration (PRO.CATG=WAVE)
P2VM	p2vm calibration (PRO.CATG=P2VM)
DARK	dark calibration (PRO.CATG=DARK)
WAVELAMP	spectrum of Argon, with position of lines
DISP_RAW (>50)	raw dispersion

## Output

PRO.CATG	short description
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DISP_VIS	intermediate product
DISP_MODEL	dispersion model of FDDL

## Parameters

Name	short description
–static-name	Use static names for the products (for ESO). [FALSE]
–preproc-file	Save the PREPROC intermediate product. [FALSE]
–p2vmreduced-file	Save the P2VMRED intermediate product. [FALSE]
–vis-file	Save the VIS intermediate product. [FALSE]
–nsmooth-snr-ft	Number of samples to average coherently when computing the real-time SNR and GDELAY of the FT (shall correspond to the atmospheric coherence time). The integration window runs from -nsmooth -> +nsmooth. [5]
–snr-min-ft	SNR threshold to accept FT frames (>0). It raises the first bit (<<0) of column REJECTION_FLAG of FT. [30.0]
–global-state-min-ft	Minimum OPDC state to accept FT frames (>=0) It raises the second bit (<<1) of column REJECTION_FLAG of FT. [2.0]
–global-state-max-ft	Maximum OPDC state to accept FT frames (>=0) It raises the second bit (<<1) of column REJECTION_FLAG of FT. [4.0]
–state-min-ft	Minimum OPDC state per baseline to accept FT frames (>=0) It raises the second bit (<<1) of column REJECTION_FLAG of FT. [1.0]
–tracking-min-sc	Minimum ratio of accepted FT frames in order to accept a SC frames (0..1), that is, for each SC DIT, the fraction of the time the REJECTION_FLAG of the FT is not 0. It raises the first bit (<<0) of column REJECTION_FLAG of SC. [0.8]
–vfactor-min-sc	vFactor threshold to accept SC frame (0..1). [0.8]
–use-met-zero	Flag to activate metrology zero calculation in OPD_DISP. If disabled all metrology zeroes are set to zero. [TRUE]
–use-tel-met	Flag to use telescope metrology in IMAGING_REF calculation. If disabled, the default, fiber coupler metrology is used instead. [FALSE]
–max-frame	Maximum number of frames to integrate coherently into an OIFITS entry. [10000]
–force-same-time	Force all baseline/quantities to have strickly the same TIME and MJD columns. [FALSE]
–debias-sc	Subtract the V2 bias from SC. [TRUE]
–debias-ft	Subtract the V2 bias from FT. [TRUE]
–nboot	Number of bootstraps to compute error (1..100). [1]

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–vis-correction-sc	Correction of SC visibility from losses due to long integration, using the measured visibility losses with the FT (VFACTOR and/or PFACTOR) or by forcing the SC visibilities to match those of the FT (FORCE). Possible choices are: <VFACTOR   PFACTOR   VFACTOR_PFACTOR   FORCE   NONE> [NONE]
–phase-ref-sc	Reference phase used to integrate the SC frames. Use a self-estimate of the phase, fitted by poly. (SELF_REF) Use the FT phase only, interpolated in lbd (PHASE_REF) Use the FT+MET-SEP.UV phase (IMAGING_REF). <SELF_REF   PHASE_REF   IMAGING_REF   AUTO   NONE> [AUTO]
–output-phase-sc	With DIFFERENTIAL, the mean group-delay and mean phases are removed from the output VISPHI in the final OIFITS file. With ABSOLUTE, the VISPHI is kept unmodified. <DIFFERENTIAL   ABSOLUTE   AUTO> [AUTO]

## 7.11 gravity\_piezo

This recipe compute the response (open loop transfer function) of the piezo actuators used to fringe-track in GRAVITY.

1. Compute the piezo TF QC parameter\* Write product

### Input

DO.CATG	short description
PIEZOTF_RAW	dedicated observations (DPR.CATG=PIEZOTF)

### Output

PRO.CATG	short description
PIEZOTF	Response of the piezo

### Parameters

Name	short description
–static-name	Use static names for the products (for ESO). [FALSE]

### Quality control

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QC in PIEZOTF	short description
FT KAL PZ_FIT	Standard deviation of the residual of the fit of the piezo response [rad].
FT KAL PX_GAIN	Static gain of Piezo number X [rad/Volts]
FT KAL PX_DELAY	Pure delay of Piezo number X [ms]
FT KAL PX_STDEV	standard deviation error between the value calculated and the value which are used by the Kalman RTC [rad]
FT KAL PX_RESPY	Response value of Piezo number X at step number Y (AR5 decomposition) [rad/Volts].

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## 8 Re-creating the Static Calibration

### 8.1 Dispersion model

The **DISP\_MODEL** static calibration can be recomputed with the recipes **gravity\_wavelamp** and **gravity\_disp**. The principle is to accurately measure the interferometric phases obtained for various position of the FDDL (= various stretching of the fibers) at the wavelengths of known Argon lines. The following dedicated RAW data are required:

**WAVELAMP** is a spectrum of the internal argon lamp.

**DISP** are interferometric observations of the internal source for various position of the FDDL (= different stretch of the fibers).

### 8.2 Earth Orientation Parameters

The **EOP\_PARAM** static calibration can be recomputed with the recipe **gravity\_retrieve\_eop**, which shall query the IERS webpage to obtain the best estimate of the past and futur EOP.

### 8.3 Metrology diode positions

There is no recipe to create a new calibration file, but the **DIODE\_POSITION** static calibration can be update by editing the fits file.

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## 9 Detailed description of the data content

### 9.1 Recommended tools to browse data

RAW files can be conveniently opened with the last version of *QFitsView* [2] from Thomas Ott.

OIFITS product files can be conveniently open with the last version of *OIFits Explorer* [1] from the JMMC.

The consortium has built a python script to visualise most of the GRAVITY data, *run\_gravi\_visual.py*.

### 9.2 Table structure common to all data

The INSNAME header keyword specifies the combiner to which a table refers to, and thus allows to cross-reference with other tables. The EXTVER keyword specifies the instance of a table repeated in the OIFITS file to allow fast search in the tables (see python FITS class for instance). They can take the values: GRAVITY\_SC' (10), GRAVITY\_SC\_P1' (11), GRAVITY\_SC\_P2' (12), GRAVITY\_FT' (20), GRAVITY\_FT\_P1' (21), GRAVITY\_FT\_P2' (22).

The polarisation 'P1' in output products correspond to the 'S' regions in IMAGING\_DETECTOR tables. The polarisation 'P2' in output products correspond to the 'P' regions in IMAGING\_DETECTOR tables.

The IMAGING\_DETECTOR\_SC and IMAGING\_DETECTOR\_FT tables store the detector configurations based on the VLTI interface control document [5].

The IMAGING\_DATA\_SC and IMAGING\_DATA\_FT extensions store the detector data. The SC data are stored as image list, while the FT data are stored as tables.

The OI\_WAVELENGTH tables store the wavelength table following the OIFITS standard. They shall be associated to the SC or FT using the INSNAME or EXTVER keywords.

OIFITS tables storing quantities per-beam (OI\_FLUX) have a total of NDIT x 4 rows (or NEXP x 4 rows for final product). In these tables, the four beams are always ordered following 12341234...

OIFITS tables storing quantities per-baseline (OI\_VIS, OI\_VIS2) have a total of NDIT x 6 rows (or NEXP x 6 rows for final product). In these tables, the six baselines are always ordered following 123456123456... The baselines 1 to 6 are always the pair of the beams 1-2,1-3,1-4,2-3,2-4,3-4.

### 9.3 RAW calibration data

RAW calibration data are set of data acquired on internal calibration source to be reduced by the recipe *gravi\_all\_dark* and *gravi\_all\_p2vm* in order to produce master calibration frame (DARK, FLAT, BAD PIXEL and WAVE maps) characterising the detector pixels and P2VM.

The data contain the following tables :

**OPTICAL\_TRAIN** : Optical train configuration (see [5])

**IMAGING\_DATA\_ACQ** : Data of the imaging camera (image cube)

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**IMAGING\_DETECTOR\_SC** : Configuration of the SC detector

**IMAGING\_DETECTOR\_FT** : Configuration of the FT detector

**IMAGING\_DATA\_SC** : Images of the SC camera (image cube)

**IMAGING\_DATA\_FT** : Images of the FT camera

**OPDC** : OPD Controller data (fringe tracker)

**FDDL** : Fiber Delay Line position

**METROLOGY** : Metrology data

### **IMAGING\_DETECTOR\_SC and IMAGING\_DETECTOR\_FT**

The REGNAME column must refer to an output of the integrated optic. It is defined as the following [1..3][2..4]-[A,B,C,D]-[S-P]. The 2 first numbers define the 2 entrance ports connected to the output, the median letter correspond to the phase shift A, B, C or D, and the final letter is the polarisation of the region (S or P). Ex : 13-A-S is the A output of the T1-T3 pair with the polarisation S. The IMAGING\_DETECTOR\_SC tables contain the following columns:

Column	Size	Unit	Description
REGION	I		The region number that is being described by this row.
DETECTOR	I		The detector that is on this region, index defined in INS_DESCRIPTION.
CORRELATION	I		Correlation type: 0=background (no signal), 1=photometric, 2=interferometric.
REGNAME	16A		Detector region name, to match the IMAGING_DATA table.
CENTER	2I	PIXEL	This gives the position of the centre of the spectrum in the x and y dimension.
LEFT	2I	PIXEL	SC ONLY - This gives the position of the left of the spectrum in the x and y dimension.
HALFLEFT	2I	PIXEL	SC ONLY -This gives the position of the halfleft of the spectrum in the x and y dimension.
RIGHT	2I	PIXEL	SC ONLY - This gives the position of the right of the spectrum in the x and y dimension.
HALFRIGHT	2I	PIXEL	SC ONLY - This gives the position of the half right of the spectrum in the x and y dimension.

### **IMAGING\_DATA\_FT**

The IMAGING\_DATA\_FT tables contain the following columns:

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Column	Size	Unit	Description
REGION	I		The region number that is being described by this row.
REGNAME	16A		Detector region name, to match the IMAGING_DATA table.

## OPDC

This table contains the data coming from the OPD controller. It is mainly the command applied to the PIEZO and VLTi delay lines.

The OPDC tables contain the following columns:

Column	Size	Unit	Description
TIME	J	$\mu s$	Time tag for this exposure, the effective centroid from the MJD_OBS date.
STATE	J		
STEPS	J		
BASELINE_STATE	J		
PIEZO_DL_OFFSET	4E	m	
VLTi_DL_OFFSET	4E	m	
KALMAN_PIEZO	4E	rad	
OPD	6E	rad	
KALMAN_OPD	6E	rad	

## FDDL

This table contains the data coming from the FDDL controller. It is mainly the command applied to the fibered differential delay lines.

The FDDL tables contain the following columns:

Column	Size	Unit	Description
TIME	J	$\mu s$	Time tag for this exposure, the effective centroid from the MJD_OBS date.
FT_POS	4E	V	
SC_POS	4E	V	
OPL_AIR	4E	m	

## METROLOGY

This table contains metrology measurement: phase differences between reference star and target star as function of time.

The METROLOGY tables contain the following columns:

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Column	Size	Unit	Description
TIME	J	$\mu s$	Time tag for this exposure, the effective centroid from the MJD_OBS date.
VOLT	80E	V	
POWER_LASER	E	mV	
LAMBDA_LASER	E	m	

## 9.4 RAW science data

RAW science data are produced during on sky observation of calibrator or science target by the instrument. They are reduced by the recipe gravity\_vis.

The data contain the following tables :

**ARRAY\_DESCRIPTION** : Description of the telescope array (see [5])

**ARRAY\_GEOMETRY** : Positions of the used telescope (see [5])

**OPTICAL\_TRAIN** : Optical train configuration (see [5])

**IMAGING\_DATA\_ACQ** : Data of the imaging camera (image cube)

**IMAGING\_DETECTOR\_SC** : Configuration of the SC detector

**IMAGING\_DETECTOR\_FT** : Configuration of the FT detector

**IMAGING\_DATA\_SC** : Images of the SC camera (image cube)

**IMAGING\_DATA\_FT** : Images of the FT camera

**OPDC** : OPD Controller data (fringe tracker)

**FDDL** : Fiber Delay Line position

**METROLOGY** : Metrology data

## 9.5 P2VM product

Visibility to pixels matrix contains the beam combiner calibration matrix in P2VM table (transmission, coherence and phase) for the three data sources (P2VM\_SC, P2VM\_FT and P2VM\_MET).

The products contain the following tables :

**IMAGING\_DETECTOR\_SC** : copied from raw data

**IMAGING\_DETECTOR\_FT** : copied from raw data

**OI\_WAVELENGTH** : computed from the minimum and the maximum wavelength and the spectral resolution of the mode

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**OI\_FLUX** : store the internal instrument transmission, measured on the internal light, following the OIFITS standard, in arbitrary units. These tables are used to later calibrate the measured flux of the object using the spectral shape of the internal transmission.

**P2VM\_SC** : P2VM of the SC beam combiner

**P2VM\_FT** : P2VM of the FT beam combiner

**P2VM\_MET** : P2VM of the metrology

### **P2VM\_SC and P2VM\_FT tables**

The P2VM\_SC and P2VM\_FT tables contain the following columns:

Column	Size	Unit	Description
REGNAME	16A		Detector region name, to match the IMAGING_DATA table.
TRANSMISSION	$\text{ntel} \times \text{nwave}$ [E]		For each region (= output of the combiner), a $\text{ntel} \times \text{nwave}$ image with the transmission of each input beam in this region. Since the combination scheme is pairwise, normally only 2 rows of this image shall be non-zero.
COHERENCE	$\text{nbase} \times \text{nwave}$ [E]		For each region (= output of the combiner), a $\text{nbase} \times \text{nwave}$ image with the instrumental visibility of each pair of input beam in this region. Since the combination scheme is pairwise, normally only one single rows of this image shall be non-zero.
PHASE	$\text{nbase} \times \text{nwave}$ [E]		For each region (= output of the combiner), a $\text{nbase} \times \text{nwave}$ image with the instrumental phase in radian of each pair of input beam in this region. Since the combination scheme is pairwise, normally only one single rows of this image shall be non-zero.
C_MATRIX	$\text{nbase} \times \text{nwave}$ [E]		Normalisation matrix

## **9.6 \*\_VIS and \*\_TF products**

The files with PRO.CATG=\*\_VIS and \*\_TF follow the OIFITS standard, version 2. All information can be found in [4].

The OI\_VIS, OI\_VIS2 and OI\_T3 tables contain one row per baseline and per corresponding RAW exposure, that is all the frames from the individual exposure are averaged together.

The OI\_FLUX tables contain one row per telescope and per corresponding RAW exposure.

The OIFITS tables are associated to the SC or FT using the INSNAME (and/or EXTVER) keywords.

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## 9.7 SPECTRUM, PREPROC products

These are intermediate products used to debug the pipeline.

Both files contain the extracted spectra of each output of the combiners. In SPECTRUM, the spectra are in pixel space, thus on different wavelength grids. In PREPROC, the spectra have been re-interpolated into a common wavelength grid.

The products contain the following tables :

**IMAGING\_DETECTOR\_SC/FT** : copied from raw data

**SPECTRUM\_DATA\_SC/FT** : Computed spectra in pixels space for SPECTRUM product, or re-interpolated in PREPROC product.

**SPECTRUM\_FLAT\_SC** : Computed spectra from the FLAT in pixels space for SPECTRUM product, or re-interpolated in PREPROC product.

**OI\_WAVELENGTH** : Only for PREPROC file, this table is copied from the WAVE used for re-interpolation.

### Columns in the SPECTRUM\_DATA tables

Column	Size	Unit	Description
TIME	J	$\mu s$	time of the frame, in [us], from the PRC.ACQ.START time from header (RMN recording start).
DATAi	NWAVE*D	e	The spectrum of the flux from output i of the combiner.
DATAERRi	NWAVE*D	e	The spectrum of the theoretical error of the flux from output i of the combiner, including detector and photonic variances.

### Columns in the SPECTRUM\_FLAT\_SC tables

Column	Size	Unit	Description
DATAi	NWAVE*D	e	The spectrum of the flux from output i of the combiner.
DATAERRi	NWAVE*D	e	The spectrum of the theoretical error of the flux from output i of the combiner, including detector and photonic variances.

## 9.8 \*\_P2VMRED products

The files with PRO.CATG=\*\_P2VMRED use elements of the OIFITS format [4], but are non-standard for the TIME columns. They also include many additional columns to store intermediate signal.

Beware that the OIFITS tables contain one row per frame: the number of row can be huge for the FT tables.

The product contains the following tables :



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**OI\_WAVELENGTH** : copied form the WAVE used for re-interpolation.

**OI\_TARGET** : created by the pipeline from the template parameters (see [4] for description).

**OI\_ARRAY** : created by the pipeline from ARRAY\_GEOMETRY table of the raw data (see [4] for description).

**OI\_VIS** : computed visibilitites adapted from [4] see below.

**OI\_FLUX** : computed flux adapted from [4] see below.

**METROLOGY** : copied form the RAW data

**OI\_VIS\_MET** : computed phase of the metrology see below.

**FDDL** : copied form the RAW data

**OPDC** : copied form the RAW data

If the ACQUISITION camara data are reduced :

**IMAGING\_DATA\_ACQ** : reduced images of the acquisition camera (see below)

**OI\_VIS\_ACQ** : computed data from the acquisition camera images (see below)

#### Columns in the OI\_VIS table of the SC

**TARGET\_ID** : id listed in OI\_TARGET

**TIME** [ $\mu$ s] : time of the frame, in [us], from the PRC.ACQ.START time from header (RMN recording start).

**MJD** [day] :

**INT\_TIME** [s] : integration time of this frame

**VISDATA** [e,e] : complex coherent flux of SC in this frame

**VISERR** [e,e] : theoretical complex error on the coherent flux

**UCOORD** [m] : uv-plane of this SC frame

**VCOORD** [m] : uv-plane of this SC frame

**STA\_INDEX** : station index in the OI\_ARRAY

**FLAG** : T if flagged, F if not flagged

**E\_U, E\_V, E\_W** : Local celestial {u,v,w} (East, North, Toward observer = OIFITS standard) expressed in local terrestrial (East, North, Up) at Paranal reference. It is useful for recomputing the projected baseline from physical baseline.

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**E\_Az** : Vector product of the E\_W and the Zenith directions, expressed in the local terrestrial (East, North, Up) at Paranal reference. Sitting on telescope, looking at the target, E\_Az points toward left in the horizontal plane.

**E\_Zd** : Vector product of the E\_W and E\_Az, expressed in the local terrestrial (East, North, Up) at Paranal reference. Sitting on telescope, looking at the target, E\_Az points toward Nadir in the plane perpendicular to pointing direction.

**SNR** : real-time SNR

**GDELAY\_BOOT** [m] : best GD estimate, taking into account closing triangles

**SNR\_BOOT** : best SNR estimate, taking into account closing triangles

**FIRST\_FT** : first FT frame in this SC frame

**LAST\_FT** : last FT frame in this SC frame

**NFRAME\_FT** :

**FIRST\_MET** : first MET frame in this SC frame

**LAST\_MET** : last MET frame in this SC frame

**NFRAME\_MET** :

**P\_FACTOR** : predicted square visibility loss of this SC frame due to photometric flickering (based on the real-time photometry of the FT)

**F1F2** Estimate of geometric flux of this frame.

**PHASE\_MET\_FC** [rad] : unwrapped FT-SC phase as computed by the DRS algorithm

**PHASE\_MET\_TEL** [rad] : unwrapped FT-SC phase as computed by the DRS algorithm, mean of 4 diodes

**OPD\_MET\_FC** [m] : unwrapped SC-FT delay as computed by the TAC algorithm

**OPD\_MET\_TEL** [m] : unwrapped SC-FT delay as computed by the TAC algorithm, 4 diodes

**PHASOR\_MET\_TELFC** : average over the SC DIT of the baseline difference of the respective PHASOR\_TELFC in OI\_VIS\_MET

**OPD\_MET\_FC\_CORR** :

**OPD\_MET\_TELFC\_MCORR** :

**OPD\_MET\_TELFC\_CORR** :

**VISDATA\_FT** [e,e] : <VISDATA> spectra of FT (integrated in this SC frame)

**VISVAR\_FT** [e\*\*2] : <|VISERR|\*\*2> spectra of FT (integrated in this SC frame)

**VISPOWER\_FT** [e\*\*2] : <|VISDATA|\*\*2> spectra of FT (integrated in this SC frame)

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**V\_FACTOR** : predicted square visibility loss of this SC frame (re-interpolation of V\_FACTOR\_FT on the SC wavelengths)

**V\_FACTOR\_FT** : measured visibility loss on the FT

**V\_FACTOR\_WL** : predicted square visibility loss in white light for the SC.

**OPD\_DISP** [m] : spectra of OPD introduced by fibers, including dispersion.

**GDELAY\_DISP** [m] :

**PHASE\_DISP** [m] :

**GDELAY** [m] : real-time GD computed from VISDATA

**GDELAY\_FT** [m] : real-time GD computed from VISDATA\_FT

**SELF\_REF** [rad] : self-reference phase.

**SELF\_REF\_COEFF** [rad] :

**PHASE\_REF** [rad] : reference phase from FT, actually  $-1 * \arg(\text{VISDATA\_FT})$ , re-interpolated in the SC wavelength.

**PHASE\_REF\_COEFF** [rad] : polynomial coefficients fit to  $\arg(\text{VISDATA\_FT})$  and used to extrapolate to the SC wavelengths, in units of  $(\lambda - \lambda_{mean}) / (\lambda_{max} - \lambda_{min})$

**IMAGING\_REF** [rad] : reference phase for dual-mode, which include the PHASE\_REF, the metrology and the sidereal motion.

**FRINGEDET\_RATIO** : fraction of FT frame accepted in this SC frame

**REJECTION\_FLAG** : this frame is accepted/rejected

**PUPIL\_U** [m] : lateral shift of pupil (in uv reference).

**PUPIL\_V** [m] : lateral shift of pupil (in uv reference).

**PUPIL\_W** [m] : focus shift of pupil (in uv reference).

#### Columns in the OI\_VIS table of the FT

**TARGET\_PHASE** [rad] : target phase of the loop, including the Sylvester modulation

**STATE** : baseline tracking state as reported by OPDC

**OPDC\_STATE** :

**SNR** : real-time SNR

**GDELAY\_BOOT** [m] : best GD estimate, accounting closing triangles

**SNR\_BOOT** : best SNR estimate, accounting closing triangles

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**F1F2** Estimate of geometric flux of this frame.

**SELF\_REF** [rad] : self-reference phase.

**GDELAY** [m] : real-time GD computed from VISDATA

**REJECTION\_FLAG** : this frame is accepted/rejected

#### Columns in the OI\_FLUX table of the SC

**TARGET\_ID** : id listed in OI\_TARGET

**TIME** [us] : time of the frame, in [us], from the PRC.ACQ.START time from header (RMN recording start).

**MJD** [day] :

**INT\_TIME** [s] : integration time of this frame

**FLUX** [e] : flux

**FLUXERR** [e] : theoretical error on flux

**STA\_INDEX** : station index in the OI\_ARRAY

**FLAG** : T if flagged, F if not flagged

**FIRST\_FT** : first FT frame in this SC frame

**LAST\_FT** : last FT frame in this SC frame

**NFRAME\_FT** :

**FIRST\_MET** : first MET frame in this SC frame

**LAST\_MET** : last MET frame in this SC frame

**NFRAME\_MET** :

**FIRST\_FDDL** : first FDDL frame in this SC frame

**LAST\_FDDL** : last FDDL frame in this SC frame

**NFRAME\_FDDL** :

**OPD\_MET\_FC** [m] : unwrap SC-FT delay as computed by the TAC algorithm

**OPD\_MET\_TEL** [m] : unwrap SC-FT delay as computed by the TAC algorithm, 4 diodes.

**PHASOR\_MET\_TELFC** : average over the SC DIT of PHASOR\_TELFC in OI\_VIS\_MET

**OPD\_MET\_FC\_CORR** :

**OPD\_MET\_TELFC\_MCORR** :

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#### **OPD\_MET\_TELFC\_CORR :**

**FT\_POS** [V] : mean FT FDDL strain gauge voltage during this frame

**SC\_POS** [V] : mean SC FDDL strain gauge voltage during this frame

**OPL\_AIR** [m] : optical path length calculated as the scalar product between the telescope position and the target direction

**TOTALFLUX\_SC** [e] : total flux of SC in this SC frame (integrated over spectrum)

**TOTALFLUX\_FT** [e] : total flux of FT in this SC frame (integrated over spectrum)

**FDDL** [m] : The mean of SC\_FDDL and FT\_FDDL, where these value are the FDDL strain gauge measurements, corrected from non-linearity and converted in [m].

#### **Columns in the OI\_FLUX table of the FT**

**STATE** : telescope state as reported by OPDC

#### **Columns in the OI\_VIS\_MET table**

The table has the same structure as the OI\_FLUX table, that is one row per beam (12341234124...), and thus nsample x 4 rows.

**PHASE\_FC** [rad] : phases at combiner, unwrap by pipeline algorithm (FT-SC)

**PHASE\_TEL** [rad] : 4 diodes phases at telescope, unwrap by pipeline algorithm (FT-SC)

**PHASOR\_TELFC** : metrology complex phasor of the double difference (FT-SC) and (TEL-FC)

**FLAG\_FC, FLAG\_TEL** : flags computed by TAC algorithm

**OPD\_FC** [m] : OPD at telescope, unwrap by TAC algorithm (SC-FT)

**VAMP\_FC\_FT** , **VAMP\_FC\_SC**, **VAMP\_TEL\_FT**, **VAMP\_TEL\_SC**: Volt amplitudes

**OPD\_TEL** [m] : 4 diodes OPD at telescope, unwrap by TAC algorithm (SC-FT)

**OPD\_FC\_CORR** [m] :

**OPD\_TEL\_CORR** [m] :

**OPD\_TELFC\_CORR** [m] :

**OPD\_TELFC\_MCORR** [m] :

**OPD\_PUPIL** [m] : Expected OPD introduced by the measured pupil shift, re-aligned in time with the MET sampling.

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### Columns in the OI\_VIS\_ACQ table

The table has the same structure as the OI\_FLUX table, that is one row per beam (12341234124...), and thus nsample x 4 rows.

**TIME** [us] : time of the frame, in [us], from the PRC.ACQ.START

**PUPIL\_NSPOT** : number of spot detected in the pupil sensor (maximum is 16 = 4 diodes x 4 sub-apertures).

**PUPIL\_X** [pix] : horizontal shift of pupil (in detector).

**PUPIL\_Y** [pix] : vertical shift of pupil (in detector).

**PUPIL\_Z** [pix] : focus shift of pupil (in detector).

**PUPIL\_R** [deg] : rotation of pupil diode (in detector).

**PUPIL\_U** [m] : lateral shift of pupil (in uv reference).

**PUPIL\_V** [m] : lateral shift of pupil (in uv reference).

**PUPIL\_W** [m] : focus shift of pupil (in uv reference).

**OPD\_PUPIL** [m] : Expected OPD introduced by the measured pupil shift.

### Columns in the OPDC table

**TIME** [us] : time of the frame, in [us], from the PRC.ACQ.START time from header (RMN recording start).

**STATE** : global fringe tracking state

**STEPS** : target phase modulation per baseline (scrambled), in units of  $\pi/8$

**BASELINE\_STATE** : fringe tracking state per telescope and baseline (scrambled)

**PIEZO\_DL\_OFFSET** :

**VLTI\_DL\_OFFSET** :

**VLTI\_FDDL\_OFFSET** :

**OPD** :

**KALMAN\_PREDICT** :

## 9.9 \*\_ASTROREDUCED products

This is a light version of the P2VMRED file. It is meant to develop the astrometric mode of GRAVITY.

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## 9.10 DISP\_MODEL

The data are stored in the table DISP\_MODEL. There are one line per GRAVITY beam. They are used to calculate OPD\_DISP (see section 10.22). The columns are:

**WAVE0** :  $\lambda_0$ , reference wavelength to calculate OPD\_DISP model.

**NMEAN** : Mean optical index of the SC and FT fibers. The vector contains the  $nmean_i$  coefficients such that the index at wavelength  $\lambda$  is given by :  $n(\lambda)/n(\lambda_{MET}) = \sum_i (nmean_i (\frac{\lambda_0}{\lambda} - 1)^i)$ .

**NDIFF** : Differential optical index between the SC and the FT fibers. The vector contains the  $ndiff_i$  coefficients such that the differential index at wavelength  $\lambda$  is given by :  $n(\lambda)/n(\lambda_{MET}) = \sum_i (ndiff_i (\frac{\lambda_0}{\lambda} - 1)^i)$ .

**LIN\_FDDL\_FT** : Linearity coefficients to convert the FDDL signal in [V] to stretching length in [m]. The vector contains the  $a_i$  coefficients such that  $L(V) = \sum_i a_i V^i$ .

**LIN\_FDDL\_SC** : Same for the SC.

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## 10 Algorithms

In the following,  $f$  is the index of individual DIT (that is from 0 to NDIT-1, whose typical values are 30 for SC and 300000 for FT),  $ij$  are the pixel indices on the detector ( $i$  being the spatial direction, and  $j$  being the spectral direction),  $l$  is for the spectral channel,  $o$  is the combiner output (so called region in the code, [0..23] or [0..47] if polarisations are split),  $b$  is the baseline [0..5], and  $t$  is the telescope/beam [0..4].

### 10.1 Correction of detector bias

The SC frames are corrected for the detector bias using the value of some specific pixels, supposedly non-illuminated. In LOW and MED spectral mode, the bias per frame is estimated as the mean over all the pixels of the *bias lines* interleaved between the spectra of each region.

In HIGH spectral mode, the bias per frame is estimated as the mean over all pixels of the *bias columns* at the edge of the detector.

In both case, there is thus a single, scalar bias value for the entire frame for each frame.

### 10.2 Dark map

The dark map is computed from a set of images acquired with all shutters closed and with the same exposure time as the raw image and as close in time as possible. The dark is computed for FT, SC and MET.

The dark map is the median image of this set of images.

$$D_{ij} = \text{median}_f(X_{fij}) \quad (1)$$

### 10.3 Spectrum extraction

The implemented spectrum extraction  $Y_{foj}$  from the 2D image  $X_{fij}$  is based on a profile image  $p_{oij}$ .

#### Profile definition

When computing the profile from the sequence of 4 FLAT files, the first step is to add the 4 median of the 4 files. Then for each output a Gaussian fit is performed for each column (spectral element) over the specified profile\_width pixels.

Depending of the profile-mode option the used profile can be either the gaussian fit (GAUSS), the measured pixels intensity (PROFILE), or boxcard (BOX). AUTO is the default option value and means PROFILE for LOW and MED mode, and BOX for HIGH mode.

In LOW and MED spectral modes, the profile is identical to the one observed with the sequences of FLAT files. It resembles a Gaussian function with FWHM of 1.5 pixel. To ensure the overall flux is conserved in the



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extraction, we apply the following normalization which assumes the shape of the object spectrum is perfectly matched by the profile itself:

$$p_{oij} = p_{oij} \cdot \frac{\sum_i p_{oij}}{\sum_i p_{oij}^2} \quad (2)$$

In HIGH mode, the profile is a boxcar of 6 pixels around the center of the best-fit Gaussian on the observed profile in the FLAT files. To ensure flux conservation, this boxcar is either 0 (outside) or 1 (inside).

### Bad pixels in profile

The bad pixels are forced to zero in the profile. Consequently, a profile with bad pixels will lead to a reduced amount of detected flux. This effect is calibrated by the P2VM algorithm because the P2VM coefficients and the data are affected by the same amount of flux losses. A worst, for some spectral channels, the spectra of one output (e.g A) can be forced zero if all the pixels are bad. The P2VM then relies on the remaining BCD outputs only.

### Extracted spectrum and variance for SC

$$Y_{foj} = g \sum_i (X_{fij} - S_{ij}) p_{oij} \quad (3)$$

where  $S_{i,j}$  is the mean image measured on the SKY, and  $g$  is the conversion gain from [ADU] to [e]. The sum  $\sum$  is obviously performed in the compressed spatial direction.

Introducing the photon and detector noise, the variance of the extracted spectrum is:

$$\text{var}(Y)_{foj} = g \sum_i (X_{fij} - D_{ij}) p_{oij}^2 + g^2 \sum_i \sigma_{ij}^2 p_{oij}^2 \quad (4)$$

where  $D_{i,j}$  is the mean level measured on the DARK, and  $\sigma_{ij}^2$  is the variance measured on the DARK.

If no SKY is available, it is replaced by the DARK in Eq.3. Note that this can bias the result since the background estimate will miss the true sky brightness, which is significant for long DIT and at the end of the K-band. If no DARK is available, it is replaced by the SKY in Eq.4. Note however that the number of frames in the SKY may be insufficient to properly estimate the variance, especially for the long DIT. Therefore it is strongly recommended to always reduce SC science observation with both a DARK with high statistic, *and* a SKY taken close in time and observing condition.

### Extracted spectrum and variance for FT

$$Y_{foj} = g \sum_i (X_{fij} - S_{ij}) p_{oij} \quad (5)$$

$$\text{var}(Y)_{foj} = g \sum_i (X_{fij} - S_{ij}) p_{oij}^2 + g^2 \sum_i \sigma_{ij}^2 p_{oij}^2 \quad (6)$$

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where  $g$  is the conversion gain from [ADU] to [e],  $S_{i,j}$  is the mean level measured on the SKY, and  $\sigma_{ij}^2$  is the variance measured on the SKY.

If no SKY is available, it is replaced by the DARK in Eq.5 and Eq.6. Using a DARK or SKY makes little difference for the FT because the sky brightness is negligible at the FT frame rate, and because there is always enough statistic. However, it is critical to use a DARK or SKY calibration taken *close in time*, and with *exactly* the same FT setup.

## 10.4 Wavelength calibration

### 10.4.1 Compute the phase from ABCD

To compute the phase from the A, B, C and D measurements without knowing the P2VM, the 2 quantities  $X = C - A$  and  $Y = D - B$  must be corrected to compensate for non-perpendicularities of A, B, C and D. An ellipse with equation 5 is fitted to the raw data.

$$\sqrt{(aX + bY + c)^2 + (dY + e)^2} = 1 \quad (7)$$

Knowing the fitted parameters (a, b, c, d and e), we compute the corrected  $X' = aX + bY + c$  and  $Y' = dY + e$ . The corrected points are now on a centered and normalized circle (Fig 4).

The phases are now computed as :

$$\varphi = \arctan\left(\frac{X'}{Y'}\right) \quad (8)$$

The phase values are between 0 and  $2\pi$ , to reconstruct the continuous evolution of the phases one needs to unwrap the numbers.

### 10.4.2 Evaluation of the OPD

To do the wavelength calibration we have to compute the  $OPD_{FT}$  and  $OPD_{SC}$  from the FT and SC data and the metrology measurement. This is possible because the scanning of the FT and SC FDDL are at different time scale. The relation linking  $OPD_{FT} = a\tilde{\varphi}_{FT}$ ,  $OPD_{SC} = b\tilde{\varphi}_{SC}$  and the differential metrology is the following:

$$a\tilde{\varphi}_{FT} - b\tilde{\varphi}_{SC} + c = dOPL_{MET} \quad (9)$$

We compute  $\tilde{\varphi}_{FT}(t_{FT})$  from FT data as the mean phase. This is done by computing the phase of each spectral element with ellipse method, and then computing the mean of the phase for the whole wavelengths.

We compute  $\tilde{\varphi}_{SC}(t_{FT})$  from SC data as the mean phase, by the same way, and scaled at the time of the FT data.

We compute  $dOPD_{MET}$  at the time scale of the FT data.

$$dOPD_{MET} = \varphi_{MET} * \lambda_{MET} / 2\pi$$

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$$a\tilde{\varphi}_{FT} - b\tilde{\varphi}_{SC} + c = dOPD_{MET}$$

Find a and b by fitting eq 9 on the metrology data. This equation can be written with the following matrix:

$$\begin{pmatrix} OPD_{METj}^t - OPD_{METi}^t \\ \vdots \end{pmatrix} = \begin{pmatrix} \tilde{\varphi}_{FTij}^t & -\tilde{\varphi}_{SCij}^t & 1 \\ \vdots & \vdots & \vdots \end{pmatrix} \begin{pmatrix} a \\ b \\ c \end{pmatrix}$$

$\begin{pmatrix} \tilde{\varphi}_{FT}^t & -\tilde{\varphi}_{FT}^t & 1 \\ \vdots & \vdots & \vdots \end{pmatrix}$  can be inverted via singular value decomposition and a, b and c computed as

$$\begin{pmatrix} a \\ b \\ c \end{pmatrix} = \begin{pmatrix} \tilde{\varphi}_{FTij}^t & -\tilde{\varphi}_{SCij}^t & 1 \\ \vdots & \vdots & \vdots \end{pmatrix}^{-1} \begin{pmatrix} OPD_{METj}^t - OPD_{METi}^t \\ \vdots \end{pmatrix}$$

For each baseline we compute the following

$$OPD_{FT} = a\tilde{\varphi}_{FT}$$

$$OPD_{SC} = b\tilde{\varphi}_{SC}$$

### 10.4.3 Spectral calibration

The wavelength of each spectral element is computed by comparing the measured phases of this spectral element with the realized OPD:  $OPD_{FT}$  or  $OPD_{SC}$ .

The measured phases are computed from the A, B, C and D measurements with ellipse methode.

For each computed phase we know the expected OPD,  $OPD_{FT}$  or  $OPD_{SC}$  from the metrology The slope of the phase versus OPD gives us the wavelength of the spectral element.

This wavelength is the one of the ABCD set of spectral elements for a given position, which is the barycentre of these four spectral elements. When all spectral element wavelengths are computed we have two sets of calibrated points, one for each polarization. On each of these two sets, a model of lambda versus position on the detector is fitted. And from this the wavelength of each spectral element of each spectrum is computed and put in the wavelength map.

## 10.5 Re-interpolation to a common wavelength

### Modified target wavelength for SC

For the output (region)  $o$ , let's call  $j_{ol}$  the sample just below the target wavelength  $\lambda_l$ , and  $j_{ol} + 1$  the sample just above. Of course  $j$  depends on the region because their wavelength tables are different.

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For the SC, this target wavelength is slightly modified, in a different way, for each region:

$$\lambda'_{ol} = \lambda_{o,jol} + \frac{(\lambda_l - \lambda_{o,jol})(\lambda_{o,jol+1} - \lambda_{o,jol})}{(\lambda_l - \lambda_{o,jol}) + (\lambda_{o,jol+1} - \lambda_l) \cdot \frac{F_{o,jol+1}}{F_{o,jol}}} \quad (10)$$

where  $F_{oj}$  is the flat measured on the internal light, extracted the same way as the data. This modification ensures that we later interpolate to a common *effective wavelength* for all regions. It also ensures that spectral channels whose interpolation includes a bad-pixel (forced to zero) are all set to zero.

### Modified target wavelength for FT

For the FT, we don't modify the target wavelength:

$$\lambda'_{ol} = \lambda_l \quad (11)$$

### Interpolation of flux and variance

The following coefficient  $a_{ol}$

$$a_{ol} = \frac{\lambda_{o,j+1} - \lambda'_{ol}}{\lambda_{o,j+1} - \lambda_{o,j}} \quad (12)$$

allows to linearly interpolate the fluxes:

$$Y_{fol} = a_{ol} Y_{fo,jol} + (1 - a_{ol}) Y_{fo,jol+1} \quad (13)$$

and the variances:

$$\text{var}(Y)_{fol} = a_{ol}^2 \text{var}(Y)_{fo,jol} + (1 - a_{ol})^2 \text{var}(Y)_{fo,jol+1} \quad (14)$$

## 10.6 Computation of the P2VM

The P2VM theory is inspired by the amber data reduction (Tatulli et al. 2007), which is working fine. It has been adapted to the integrated optics specificities (Lacour et al. 2008).

Figure 10.1 represents the generalized view of the transfer function of an integrated optics component.  $E_n$  is the complex electric field entering the component via input  $n$ , and  $S_k$  is the resulting field on output number  $k$ .  $T_{k,n}$  is a two dimensional complex matrix linking  $S_k$  to  $E_n$ .

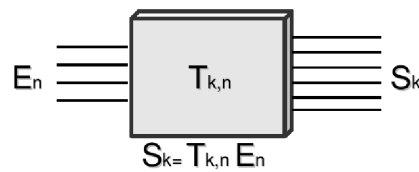


Figure 10.1: Generalization of the transfer function of an integrated optics component

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The flux  $q$  received by the detector from the output  $k$  at wavelength  $\lambda$  and instant  $t$  is written as

$$q_k^{\lambda,t} = |S_k^{\lambda,t}|^2 = \left| \sum_n T_{k,n}^{\lambda} E_n^{\lambda,t} \right|^2 \quad (15)$$

with the electric fields  $E_n^{\lambda,t}$  and  $S_k^{\lambda,t}$  as function of time and wavelength and of input  $n$  and output  $k$  respectively.  $T_{k,n}^{\lambda}$  is the complex matrix function of wavelength linking  $E_n^{\lambda,t}$  and  $S_k^{\lambda,t}$ .

With introduction of  $V_{n,m}$  (coherence of the incoming electric field) and  $C_{k,n,m}^{\lambda}$  (integrated optics conservation of light coherence) equation (7) can be developed as:

$$|S_k^{\lambda,t}|^2 = R \left[ \sum_n |T_{k,n}^{\lambda}|^2 |E_n^{\lambda,t}|^2 + \sum_n \sum_{m>n} 2T_{k,n}^{\lambda} T_{k,m}^{\lambda*} C_{k,n,m}^{\lambda} E_n^{\lambda,t} E_m^{\lambda,t*} V_{n,m}^{\lambda} \right] \quad (16)$$

or

$$\begin{aligned} |S_k^{\lambda,t}|^2 = & \sum_n |T_{k,n}^{\lambda}|^2 |E_n^{\lambda,t}|^2 + \sum_n \sum_{m>n} \Re 2T_{k,n}^{\lambda} T_{k,m}^{\lambda*} C_{k,n,m}^{\lambda} \Re E_n^{\lambda,t} E_m^{\lambda,t*} V_{n,m}^{\lambda} \\ & - \sum_n \sum_{m>n} \Im 2T_{k,n}^{\lambda} T_{k,m}^{\lambda*} C_{k,n,m}^{\lambda} \Im E_n^{\lambda,t} E_m^{\lambda,t*} V_{n,m}^{\lambda} \end{aligned} \quad (17)$$

Using the matrix expression:

$$\begin{pmatrix} |S_1^{\lambda,t}|^2 \\ \vdots \\ |S_K^{\lambda,t}|^2 \end{pmatrix} = R \left[ V2PM_C \cdot \begin{pmatrix} |E_1^{\lambda,t}|^2 \\ \vdots \\ |E_N^{\lambda,t}|^2 \\ E_1^{\lambda,t} E_2^{\lambda,t} V_{1,2} \\ \vdots \\ E_{N-1}^{\lambda,t} E_N^{\lambda,t} V_{N-1,N} \end{pmatrix} \right] = V2PM_R \cdot \begin{pmatrix} |E_1^{\lambda,t}|^2 \\ \vdots \\ |E_N^{\lambda,t}|^2 \\ R[E_1^{\lambda,t} E_2^{\lambda,t} V_{1,2}] \\ \vdots \\ R[E_{N-1}^{\lambda,t} E_N^{\lambda,t} V_{N-1,N}] \\ I[E_1^{\lambda,t} E_2^{\lambda,t} V_{1,2}] \\ \vdots \\ I[E_{N-1}^{\lambda,t} E_N^{\lambda,t} V_{N-1,N}] \end{pmatrix} \quad (18)$$

with  $N$  entries and  $K$  output. The complex  $V2PM$  is defined as:

$$V2PM_C = \begin{pmatrix} |T_{1,1}^{\lambda}|^2 & \cdots & |T_{1,N}^{\lambda}|^2 & 2T_{1,1}T_{1,2}C_{1,1,2}^{\lambda} & \cdots & 2T_{1,N-1}T_{1,N}C_{1,N-1,N}^{\lambda} \\ \vdots & & \vdots & \vdots & & \vdots \\ |T_{K,1}^{\lambda}|^2 & \cdots & |T_{K,N}^{\lambda}|^2 & 2T_{K,1}T_{K,2}C_{K,1,2}^{\lambda} & \cdots & 2T_{K,N-1}T_{K,N}C_{K,N-1,N}^{\lambda} \end{pmatrix} \quad (19)$$

Where the  $N$  first columns are the transmissions of the integrated optic, and the  $N(N-1)/2$  others are the coher-

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ences. The real V2PM matrix which can be used for visibility computing is:

$$V2PM_R = \begin{pmatrix} |T_{1,1}^\lambda|^2 & \cdots & |T_{1,N}^\lambda|^2 & R[2T_{1,1}T_{1,2}C_{1,1,2}^\lambda] & \cdots & R[2T_{1,N-1}T_{1,N}C_{1,N-1,N}^\lambda] & -I[2T_{1,1}T_{1,2}C_{1,1,2}^\lambda] \\ \vdots & \ddots & \vdots & \vdots & \vdots & \vdots & \vdots \\ |T_{K,1}^\lambda|^2 & \cdots & |T_{K,N}^\lambda|^2 & R[2T_{K,1}T_{K,2}C_{K,1,2}^\lambda] & \cdots & R[2T_{K,N-1}T_{K,N}C_{K,N-1,N}^\lambda] & -I[2T_{K,1}T_{K,2}C_{K,1,2}^\lambda] \end{pmatrix}$$

**Compute the transmissions**  $|T_{k,n}^\lambda|^2$

This is done when only the shutter n is open. So we have  $E_m^{\lambda,t} = 0 \forall m \neq n$ . Eq (3) becomes:

$$|S_k^{\lambda,t}|^2 = |T_{k,n}^\lambda|^2 |E_n^{\lambda,t}|^2 \Leftrightarrow |T_{k,n}^\lambda|^2 = \frac{|S_k^{\lambda,t}|^2}{|E_n^{\lambda,t}|^2} \quad (20)$$

To avoid that  $T_{k,n}^\lambda$  depends on the input flux, we assume that all incoming photons proceed to the exit of the optics, so:

$$\sum_k |S_k^{\lambda_0,t}|^2 \times \tilde{E}(\lambda) = |E_n^{\lambda,t}|^2 \quad (21)$$

Now  $T_{k,n}^\lambda$  can be expressed as:

$$|T_{k,n}^\lambda|^2 = \frac{\langle |S_k^{\lambda,t}|^2 \rangle_t}{\langle \sum_k |S_k^{\lambda_0,t}|^2 \rangle_t \times \tilde{E}(\lambda)} \quad (22)$$

**Compute the coherences**  $2T_{k,n}^\lambda T_{k,m}^{\lambda*} C_{k,n,m}^\lambda$

This is done when the shutter n and m are open and others closed. So we have  $E_i^{\lambda,t} = 0 \forall i \neq m, n$ .

A calibration source is used with  $V_{n,m}^\lambda = 1$ , so from eq (8) we have:

$$|S_k^{\lambda,t}|^2 = |T_{k,n}^\lambda|^2 |E_n^{\lambda,t}|^2 + |T_{k,m}^\lambda|^2 |E_m^{\lambda,t}|^2 + R[2T_{k,n}^\lambda T_{k,m}^{\lambda*} C_{k,n,m}^\lambda E_n^{\lambda,t} E_m^{\lambda,t*}] \quad (23)$$

This can be developed with  $E_n^{\lambda,t} = \sqrt{I_n^{\lambda,t}} e^{-2i\pi \frac{OPD_n^t}{\lambda}}$  as:

$$|S_k^{\lambda,t}|^2 = |T_{k,n}^\lambda|^2 I_n^{\lambda,t} + |T_{k,m}^\lambda|^2 I_m^{\lambda,t} + 2 |T_{k,n}^\lambda T_{k,m}^{\lambda*} C_{k,n,m}^\lambda| \sqrt{I_n^{\lambda,t} I_m^{\lambda,t}} \cos 2\pi \frac{OPD_{m,n}^t}{\lambda} + \varphi_{k,n,m}^\lambda \quad (24)$$

With  $OPD_{m,n}^t = OPD_m^t - OPD_n^t$  and  $\varphi_{k,n,m}^\lambda$  is the phase of  $T_{k,n}^\lambda T_{k,m}^{\lambda*} C_{k,n,m}^\lambda$ .

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This equation can be fitted by a sinusoid with 3 free parameters (a, b and c)

$$\left| S_k^{\lambda,t} \right|^2 = a_{k,m,n}^{\lambda} \cos \frac{OPD_{m,n}^t}{\lambda} 2\pi + b_{k,m,n}^{\lambda} \sin \frac{OPD_{m,n}^t}{\lambda} 2\pi + c_{k,m,n}^{\lambda} \quad (25)$$

With:

$$c_{k,m,n}^{\lambda} = \left| T_{k,n}^{\lambda} \right|^2 I_n^{\lambda,t} + \left| T_{k,m}^{\lambda} \right|^2 I_m^{\lambda,t} \quad (26)$$

$$\varphi_{k,n,m}^{\lambda} = \arctan \left[ \frac{b_{k,m,n}^{\lambda}}{a_{k,m,n}^{\lambda}} \right] \quad (27)$$

$$2 \left| T_{k,n}^{\lambda} T_{k,m}^{\lambda*} C_{k,n,m}^{\lambda} \right| \sqrt{I_n^{\lambda,t} I_m^{\lambda,t}} = \sqrt{a_{k,m,n}^{\lambda^2} + b_{k,m,n}^{\lambda^2}} \quad (28)$$

The coherences (  $2 T_{k,n}^{\lambda} T_{k,m}^{\lambda*} C_{k,n,m}^{\lambda}$  ) can be expressed by their phases and amplitudes. The phase is given by eq. (13) and the amplitude is given by eq. (14). But the amplitude depends on the  $I_n^{\lambda,t}$  which can be evaluated with eq. (12).

Eq.(12) can be expressed as a matrix equation where the  $\left| T_{k,n}^{\lambda} \right|^2$  matrix is already:

$$\begin{pmatrix} c_{1,m,n}^{\lambda} \\ \vdots \\ c_{K,m,n}^{\lambda} \end{pmatrix} = \begin{pmatrix} \left| T_{1,1}^{\lambda} \right|^2 & \cdots & \left| T_{1,N}^{\lambda} \right|^2 \\ \vdots & \ddots & \vdots \\ \left| T_{K,1}^{\lambda} \right|^2 & \cdots & \left| T_{K,N}^{\lambda} \right|^2 \end{pmatrix} \cdot \begin{pmatrix} I_1^{\lambda,t} \\ \vdots \\ I_N^{\lambda,t} \end{pmatrix} \quad (29)$$

This over determined system can be solved by inverting the matrix  $\left| T_{k,n}^{\lambda} \right|^2$  with a singular value decomposition method. And knowing  $I_n^{\lambda,t}$ , we can compute the coherences amplitudes:

$$2 \left| T_{k,n}^{\lambda} T_{k,m}^{\lambda*} C_{k,n,m}^{\lambda} \right| = \frac{\sqrt{a_{k,m,n}^{\lambda^2} + b_{k,m,n}^{\lambda^2}}}{\sqrt{I_n^{\lambda,t} I_m^{\lambda,t}}} \quad (30)$$

This should be done for each base(n, m>n couple).

## Phases calibrations

The phases  $\varphi_{k,n,m}^{\lambda}$  of the integrated optics coherences  $C_{k,n,m}^{\lambda}$  can be divided into two components: the modulation phases (ABCD-like modulation)  $\psi_{k,n,m}^{\lambda}$  and the baseline phases  $\varphi_{n,m}^{\lambda}$ :

$$\varphi_{k,n,m}^{\lambda} = \psi_{k,n,m}^{\lambda} + \varphi_{n,m}^{\lambda} \quad (31)$$

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**Modulation phases** The modulation phases  $\psi_{k,n,m}^\lambda$  are defined as the instrumental phases introduced by the beam combiner between the two interfering beams  $n$  and  $m$ . For each baseline defined by the couple of beams  $(n, m)$ , the corresponding modulations phases are defined relatively to one of the beams at the output  $k = A_{(n,m)}$  acting as a reference, such that:

$$\psi_{k,n,m}^\lambda = \psi_{k,n,m}^\lambda - \psi_{A_{(n,m)},n,m}^\lambda \quad (32)$$

**Absolute baseline phases** The baseline phases  $\varphi_{n,m}^\lambda$  are defined as the absolute instrumental phases introduced by the beam combiner on each baseline. They induce instrumental closure phases different from zero, and then bias the source closure phases.

However, the absolute values of the baseline phases cannot be measured, due to different reference phases and piston disturbances. The closure phases they induce do not depend on these biases, however. The baseline phases can be calibrated and included in the V2PM, in a way not to bias the closure phases of the source.

Thus, instead of measuring the absolute baseline phases  $\varphi_{n,m}^\lambda$ , relative baseline phases  $\tilde{\varphi}_{n,m}^\lambda$  can be determined, inducing the same closure phases as the absolute instrumental phases.

**Closure phases and relative baseline phases** Let  $\Phi_{n,m}^\lambda$  and  $\tilde{\Phi}_{n,m}^\lambda$  be the vectors of respectively the 6 absolute and the 6 relative baseline phases,  $\varphi_{n,m}^\lambda$  and  $\tilde{\varphi}_{n,m}^\lambda$ , for the apertures  $(n, m) \in [301A?]0, 3[301B?]^2$ :

$$\Phi_{n,m}^\lambda = (\varphi_{0,1}^\lambda \varphi_{0,2}^\lambda \varphi_{0,3}^\lambda \varphi_{1,2}^\lambda \varphi_{1,3}^\lambda \varphi_{2,3}^\lambda)^T \quad (33)$$

$$\tilde{\Phi}_{n,m}^\lambda = (\tilde{\varphi}_{0,1}^\lambda \tilde{\varphi}_{0,2}^\lambda \tilde{\varphi}_{0,3}^\lambda \tilde{\varphi}_{1,2}^\lambda \tilde{\varphi}_{1,3}^\lambda \tilde{\varphi}_{2,3}^\lambda)^T \quad (34)$$

Let  $\Xi_{n,m,l}^\lambda$  be the vector of the 4 resulting closure phases  $\xi_{n,m,l}^\lambda$  between the 3 apertures  $(n, m, l) \in [301A?]0, 3[301B?]^3$ :

$$\Xi_{l,n,m}^\lambda = (\xi_{0,1,2}^\lambda \xi_{0,1,3}^\lambda \xi_{0,2,3}^\lambda \xi_{1,2,3}^\lambda)^T \quad (35)$$

such that:

$$\xi_{n,m,l}^\lambda = \varphi_{n,m}^\lambda + \varphi_{m,l}^\lambda - \varphi_{n,l}^\lambda \quad (36)$$

Three of these closure phases are independent, and the fourth is related to the other by:

$$\xi_{0,1,2}^\lambda + \xi_{0,2,3}^\lambda = \xi_{0,1,3}^\lambda + \xi_{1,2,3}^\lambda \quad (37)$$

Generalizing relation (22) to the vectors of closure phases and baseline phases leads to equation (24):

$$\Xi_{n,m}^\lambda = M \Phi_{n,m}^\lambda \quad (38)$$



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with the matrix M:

$$M = \begin{pmatrix} 1 & -1 & 0 & 1 & 0 & 0 \\ 1 & 0 & -1 & 0 & 1 & 0 \\ 0 & 1 & -1 & 0 & 0 & 1 \\ 0 & 0 & 0 & 1 & -1 & 1 \end{pmatrix} \quad (39)$$

The relative baseline phases  $\tilde{\varphi}_{n,m}^\lambda$  must result from a linear operation of the known closure phases, and lead to the same closure phases  $\xi_{n,m,l}^\lambda$ . Therefore the vector  $\tilde{\Phi}_{n,m}^\lambda$  must be linked to the closure phases  $\Xi_{n,m,l}^\lambda$  by a matrix N such that:

$$\tilde{\Phi}_{n,m}^\lambda = N \Xi_{n,m}^\lambda \quad (40)$$

and verify the same equation as(24):

$$\Xi_{n,m}^\lambda = M \tilde{\Phi}_{n,m}^\lambda \quad (41)$$

Thus, combining equations (26) and (27), the relative baseline phases are defined by the matrix N such that:

$$\Xi_{n,m}^\lambda = MN \Xi_{n,m}^\lambda \quad (42)$$

N is not unique and we suggest to use the N matrix such that:

$$N = \frac{1}{4} M^T = \frac{1}{4} \begin{pmatrix} 1 & 1 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & -1 & -1 & 0 \\ 1 & 0 & 0 & 1 \\ 0 & 1 & 0 & -1 \\ 0 & 0 & 1 & 1 \end{pmatrix} \quad (43)$$

Equation (26) easily leads to the vector of relative baselines phases:

$$\tilde{\Phi}_{n,m}^\lambda = \frac{1}{4} \begin{pmatrix} \xi_{0,1,2}^\lambda + \xi_{0,1,3}^\lambda \\ -\xi_{0,1,2}^\lambda + \xi_{0,2,3}^\lambda \\ -\xi_{0,1,3}^\lambda + \xi_{0,2,3}^\lambda \\ \xi_{0,1,2}^\lambda + \xi_{1,2,3}^\lambda \\ \xi_{0,1,3}^\lambda - \xi_{1,2,3}^\lambda \\ \xi_{0,2,3}^\lambda + \xi_{1,2,3}^\lambda \end{pmatrix} \quad (44)$$

**Compute the closure phases** This is done when all the shutters are open together, with a calibration source with  $V_{n,m}^\lambda = 1$ . Using an intermediate V2PM with null instrumental closure phases and baseline phases, from the intensities  $q_k^{\lambda,t}$  we can compute the vector (eq. (4)):

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$$\begin{pmatrix} |E_1^{\lambda,t}|^2 \\ \vdots \\ |E_N^{\lambda,t}|^2 \\ R[E_1^{\lambda,t} E_2^{\lambda,t} \exp(i\varphi_{1,2}^\lambda)] \\ \vdots \\ R[E_{N-1}^{\lambda,t} E_N^{\lambda,t} \exp(i\varphi_{N-1,N}^\lambda)] \\ I[E_1^{\lambda,t} E_2^{\lambda,t} \exp(i\varphi_{1,2}^\lambda)] \\ \vdots \\ I[E_{N-1}^{\lambda,t} E_N^{\lambda,t} \exp(i\varphi_{N-1,N}^\lambda)] \end{pmatrix} \quad (45)$$

The phases  $\varphi_{n,m}^\lambda$  can be expressed by the equation:

$$\varphi_n^{\lambda,t} + \varphi_m^{\lambda,t} + \varphi_{n,m}^\lambda = \arctan \left( \frac{I[E_n^{\lambda,t} E_m^{\lambda,t} \exp(i\varphi_{n,m}^\lambda)]}{R[E_n^{\lambda,t} E_m^{\lambda,t} \exp(i\varphi_{n,m}^\lambda)]} \right) \quad (46)$$

With  $\varphi_n^{\lambda,t}$  the phase of the electric field  $E_n^{\lambda,t}$ . Equation (24) therefore leads to the instrumental closure phases, free of the electric fields phases  $\varphi_n^{\lambda,t}$ . The relative baseline phases  $\tilde{\varphi}_{n,m}^\lambda$  can then be deduced from equation (30).

## 10.7 Extraction of the coherent fluxes and telescope fluxes via P2VM

The fluxes of each telescope  $F_{ftl}$  and the complex coherent flux of each base  $R_{fbl} + iI_{fbl}$  are extracted from a matricial analysis of the profiles, based on the P2VM calibration

$$(F_{ftl}, R_{fbl}, I_{fbl}) = P2VM_{b/tl}^o \times Y_{fol} \quad (47)$$

The variances are propagated assuming no correlation between the input  $Y_{fol}$ .

$$(\text{var}(F)_{ftl}, \text{var}(R)_{fbl}, \text{var}(I)_{fbl}) = (P2VM_{b/tl}^o)^2 \times \text{var}(Y)_{fol} \quad (48)$$

The  $P2VM$  is a well conditioned matrix thanks to the design of the integrated beam combiner. To demonstrate the underlying reasoning, let's consider a perfect  $P2VM$ . The four regions related to baseline  $b$  (say 0, 1, 2, 3, also called ABCD regions of baseline  $b$ ) can be combined together to build the following quantities:

- $R_{fbl} = Y_{f0l} - Y_{f2l}$ ,
- $I_{fbl} = Y_{f1l} - Y_{f3l}$  and
- $F_{ft1l} + F_{ft2l} = Y_{f0l} + Y_{f1l} + Y_{f2l} + Y_{f3l}$ .

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The two first are directly the complex coherent flux of baseline  $b$ , while the latter, combined with the constraints of the 5 other baselines, easily solve for the flux  $F_{fbl}$  of individual beams. In practice, the actual  $P2VM$  matrix takes into account the exact interferometric phase-shift between the four ABCD regions, and the relative photometric throughput.

## 10.8 Computation of SNR

### Individual SNR

The Signal to Noise Ratio (SNR) of each baseline and each frame of the the FT is computed using a running mean of the complex coherent flux over 10 consecutive samples. The complex coherent flux of the two polarisations, if any, are also averaged together after having recentered them to a common mean phase.

$$SNR_{fb} = \frac{(\sum_{f_r, l} R_{f_r, bl})^2 + (\sum_{f_r, l} I_{f_r, bl})^2}{\sum_{f_r, l} \text{var}(R)_{f_r, bl} + \sum_{f_r, l} \text{var}(I)_{f_r, bl}} \quad (49)$$

where  $f_r$  is the  $f$  index running in the interval  $\in \{f - 5, f + 5\}$  in order to implement the smoothing over 10 samples.

### Bootstrapped SNR

If fringes are detected on two consecutive baselines, then, by nature of light, fringes are detected on the closing baseline. The purpose of bootstrapping is to increase the confidence on the signal for the baselines with lowest SNR (whose SNR may well be null for astrophysical reason), by looking at these closing baseline.

A “bootstrapped” SNR is computed for each baseline and each frame, as the maximum between the SNR of this baseline and all closing triangles. For instance for the baseline  $b = b_{ij}$  among the beams  $i, j, k, l$ :

$$SNRB_{fb_{ij}} = \max\{ SNR_{fb_{ij}}, \min\{SNR_{fb_{ik}}, SNR_{fb_{kj}}\}, \min\{SNR_{fb_{il}}, SNR_{fb_{lj}}\} \} \quad (50)$$

The quantities SNR and SNRB are also computed for the SC, although they are not used in the processing.

## 10.9 Computing the vFactor

The purpose of the vFactor is to estimate the visibility loss of each individual SC frame due the phase jittering, from an analysis of the FT real-time data. This visibility loss is derived as the ratio between the coherent integration (squared norm of complex sum over DITs) and the incoherent integration (sum over DITs of complex squared norm) of the complex coherent flux of FT, across each SC DIT.

A white-light vFactor is first computed for each SC frame  $f$  with the FT data:

$$v_{fb} = \frac{(\sum_{f_r, l} R_{f_r, bl})^2 + (\sum_{f_r, l} I_{f_r, bl})^2 - \sum_{f_r, l} \text{var}(R)_{f_r, bl} - \sum_{f_r, l} \text{var}(I)_{f_r, bl}}{\sum_{f_r, l} (\sum_l R_{f_r, bl})^2 + \sum_{f_r, l} (\sum_l I_{f_r, bl})^2 - \sum_{f_r, l} \text{var}(R)_{f_r, bl} - \sum_{f_r, l} \text{var}(I)_{f_r, bl}} \times \frac{1}{n_{f_r}} \quad (51)$$

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where the sum over  $l$  is over the 6 spectral channels of the FT and the sum over  $f_{\tau}$  is over the FT frames acquired *during* the corresponding SC frame. This white-light vFactor at  $\lambda_0$  (the central wavelength of the FT) is then extrapolated to the SC channels with:

$$\tilde{v}_{fbl} = \exp\left(-\ln(v_{fb}) \frac{\lambda_0^2}{\lambda_l^2}\right) \quad (52)$$

This vFactor correction is proved to be very efficient as long as the FT astrophysical visibility remain larger than 0.1. For fully resolved baselines, the vFactor results into a indefinit 0/0 ratio. In such a situation, and if on-axis, one could simply rescale the SC visibilities to the one of the FT (see options of the recipes). In off-axis case with a fully resolved object on the FT, there is not much to be done however.

## 10.10 Computing the pFactor

The purpose of the pFactor is to estimate the visibility loss of each individual SC frame due to flux flickering, from an analysis of the FT real-time flux data. This visibility loss is derived as the ratio between the sum over DITs of the geometry mean, and the geometric mean of the sum over DITs of the photometric flux of FT, across each SC DIT.

We compute a white-light pFactor with the following formula:

$$p_{bf} = \frac{\left[ \sum_{f_{\tau}} \sqrt{(\sum_l \text{flux}_{f_{\tau}t_1 l})(\sum_l \text{flux}_{f_{\tau}t_2 l})} \right]^2}{(\sum_{f_{\tau}l} \text{flux}_{f_{\tau}t_1 l})(\sum_{f_{\tau}l} \text{flux}_{f_{\tau}t_2 l})} \quad (53)$$

This pFactor is computed in the P2VMRED product but not used so far.

## 10.11 Frame rejection

A FT frame is rejected if any of the conditions are met:

- its bootstrapped  $SNRB$  is below the threshold.
- the OPDC state of this baseline is below the threshold. The OPDC states are: 1 = IDEL, 2 = GD\_TRACKING, 3 = PHASE\_TRACKING, 4 = SEARCHING, 5 += internal calibrations.

A SC frame is rejected if any of the conditions are met:

- the fraction of accepted FT frame during this SC frame is below the threshold.
- its computed vFactor is below the threshold.

The frame selection is done on a per-baseline basis. That is the baselines have a different selection map, and thus will have a different effective time after the averaging process.

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## 10.12 Phase referencing

### Self-referencing the FT phase

The phase reference of a FT frames is the running mean phase of the FT itself over few samples:

$$P\_REF_{fbl} = \arctan\left(\sum_{f_r} I_{f_r, bl}, \sum_{f_r} R_{f_r, bl}\right) \quad (54)$$

where  $f_r$  is in the interval  $\in \{f - 3, r + 3\}$ , excluding  $f_r = f$  to avoid biases. Note that this phase is not unwrapped neither temporally nor spectrally (SNR too low, and FT supposed to be near constant phase all the time thanks to real-time tracking).

### Referencing the SC phases in single case

The phase reference of a SC frame is the mean phase of the FT during this SC frame:

$$P\_REF_{fbl} = \arctan\left(\sum_{f_{FT}} I_{f_{FT}, bl}, \sum_{f_{FT}} R_{f_{FT}, bl}\right) \quad (55)$$

where the sum over  $f_{FT}$  is over the FT frames acquired during the corresponding SC frame.

This  $P\_REF$ , which have 6 spectral channels only, is interpolated/extrapolated into the wavelengths of the SC with a polynomial fit of order 2 (after properly unwrapping the phase along the spectral direction).

### Referencing the SC phases in dual case

In case of dual-field observation, the previous reference phase is modified to account for the sidereal motion of the binary separation (dE, dN) and the metrology measurements:

$$P\_REF\_IMG_{fbl} = P\_REF_{fbl} + \frac{2\pi}{\lambda_l} (UCOORD_{fb} dE + VCOORD_{fb} dN - OPD\_DISP_{fbl}) \quad (56)$$

## 10.13 Geometric flux

The geometric flux of a baseline is the product of the photometric fluxes of the two beams of this baseline. It is needed to then normalise the complex coherent fluxes into complex visibilities.

### For the FT

The FT real-time photometry is affected by large photometric fluctuations, which make it going near zero (flux loss event) or even going to negative values because of noise. Since the geometric flux will enter the visibility normalisation in the denominator, we have to avoid as much as possible these near-zero events.

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The photometric fluctuations are highly corrected in the spectral direction. On the other side, the important property of the fluctuations to be extracted are the temporal correlations. Therefore we first compute a broad-band sum of the real-time flux of each beam, that we is temporally smooth:

$$F'_{ft} = \frac{\sum_{f_r, l} F_{f_r, tl}}{11} \quad (57)$$

where  $f_r$  is in the interval  $\in \{f - 5, f + 5\}$  (time smoothing). We also compute a normalized time-averaged spectrum for each beam:

$$F''_{lt} = \frac{\sum_f F_{ftl}}{\sum_{fl} F_{ftl}} \quad (58)$$

Only then the geometric mean is computed from these two quantities:

$$FF_{fbl} = F'_{ft_1} F''_{f, t_1 l} \times F'_{ft_2} F''_{f, t_2 l} \quad (59)$$

### For the SC

For the science, the geometric flux is simply computed as:

$$FF_{fbl} = F_{f, t_1 l} \times F_{f, t_2 l} \quad (60)$$

## 10.14 Averaged flux estimator

The previous sections describe how the real-time quantities are extracted from every single FT and SC frame. We here describe the process of averaging these real-time quantities into final product. For the flux, all frames are simply co-added. There is no frame selection at all.

$$\widetilde{\text{flux}}_{tl} = \sum_f F_{ftl} \quad (61)$$

Hence the final flux  $\widetilde{\text{flux}}_{tl}$  is the *sum* of all electron-events collected during the entire exposure and across all regions, for the beam  $t$  at channel  $l$ .

## 10.15 Averaged complex visibility estimator

For a given baseline, the averaged is computed only with accepted frames of this baseline.

The complex coherent flux vector is first rotated with the computed reference phase P\_REF (or with P\_REF\_IMG in the case of dual-observations):

$$R'_{fbl} = \cos(P\_REF_{fbl}) R_{fbl} - \sin(P\_REF_{fbl}) I_{fbl} \quad (62)$$

$$I'_{fbl} = \sin(P\_REF_{fbl}) R_{fbl} + \cos(P\_REF_{fbl}) I_{fbl} \quad (63)$$

The visibilities of each frame are averaged together accounting for the visibility loss expected from the vFactor (only for SC, that is  $v_{fbl} = 1.0$  for FT). Note that the coherent flux and the photometric flux are actually averaged first, before normalisation. The noise property is better than simply averaging the real-time normalised visibilities (Cauchy statistic).

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### Visibility amplitude

$$\widetilde{\text{visAmp}}_{bl} = \frac{\sqrt{(\sum_f R'_{fbl})^2 + (\sum_f I'_{fbl})^2}}{\sum_f \sqrt{FF_{fbl} v_{fbl}}} \quad (64)$$

### Visibility phase

$$\widetilde{\text{visPhi}}_{bl} = \arctan\left(\sum_f I'_{fbl}, \sum_f R'_{fbl}\right) \quad (65)$$

The mean spectral slope (stored in the GDELAY quantity) and mean spectral value (stored in the PHASE quantity) are removed from the VISPHI quantity.

## 10.16 Average squared visibility estimator

The square visibilities of each frame are averaged together accounting for the visibility loss expected from the vFactor (only for SC, that is  $v_{fbl} = 1.0$  for FT).

For a given baseline, the averaging is performed only with accepted frames of this baseline.

$$\widetilde{\text{vis2}}_{bl} = \frac{\sum_f R_{fbl}^2 + \sum_f I_{fbl}^2 - \sum_f \text{var}(R)_{fbl} - \sum_f \text{var}(I)_{fbl}}{\sum_f (FF_{fbl} v_{fbl})} \quad (66)$$

## 10.17 Average closure-phase estimator

The averaged bispectrum of triplet  $b_{ijk}$  is computed as the coherent integration of the bispectrum of each frame:

$$\widetilde{B}_{b_{ijk}l} = \sum_f (R_{fb_{ij}l} + i I_{fb_{ij}l}) \cdot (R_{fb_{jk}l} + i I_{fb_{jk}l}) \cdot (R_{fb_{ik}l} - i I_{fb_{ik}l}) \quad (67)$$

For a given triplet, the integration is performed only with frames for which *all* three baselines forming the triangles are accepted.

### Bispectrum phase

The closure phase is computed:

$$\widetilde{\text{t3Phi}}_{b_{ijk}l} = \arctan(\widetilde{B}_{b_{ijk}l}) \quad (68)$$

### Bispectrum amplitude

The bispectrum amplitude is also computed. However this quantity has not been verified yet.

$$\widetilde{\text{t3Amp}}_{bl} = \frac{\widetilde{B}_{b_{ijk}l}}{\sum_f (F_{ft_{il}} F_{ft_{jl}} F_{ft_{kl}} \sqrt{v_{fb_{ij}l} v_{fb_{ik}l} v_{fb_{jk}l}})} \quad (69)$$

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## 10.18 Uncertainty on average quantities

The uncertainty on average quantities is computed by bootstrapping over the accepted frames. Basic fundamentals about this technic can be in the numerical recipes book, section 15.6.

See also: [https://en.wikipedia.org/wiki/Bootstrapping\\_\(statistics\)](https://en.wikipedia.org/wiki/Bootstrapping_(statistics))

The implementation of the bootstrapping method makes use of *segmentation* when the number of frame is larger than 100, or of *Monte-Carlo* when the number of frame is smaller than 5.

### Segmentation (mostly for FT)

When the number of frames is larger than 100, the dataset is first split into a smaller number of *segments* (typically 20 to 100). First integration is done inside the segments. The final variance is estimated by bootstrapping over the segments. The number of segments does change the temporal sampling of the bootstrap, and thus the estimation of the uncertainties. We choose the number of segment so that each is about 1s length.

Note that this is mostly relevant for the FT, since the SC has often less than 100 frames (so each frame is a segment).

### Monte-Carlo (mostly for very long DIT on SC)

When the number of frames is smaller than 5, the bootstrap method provides unrealistically small uncertainties. Hence the dataset is complemented with few fake frames (up to 5), on which a random realisation of the theoretical noise is added, using the theoretical variance.

This noise is added on the correlated flux quantity only, not on the photometric fluxes, vFactor, reference phase... Moreover it is clear that Monte-Carlo propagates the *fundamental* uncertainties only (photon and detector noise), but not the *atmospheric* noises (effect of injection fluctuation, tracking quality fluctuation).

As a matter of fact, the final uncertainty when the number of frames is very low can still be under-estimated.

## 10.19 Calibration with the TF

### From CAL to TF estimations

For every observation  $c$  of an calibration star (VIS\_CAL), the visibilities are converted into VIS\_TF by dividing the VISAMP quantities by the expected visibility, accounting for the provided diameter. The uncertainty on the diameter is not propagated to the VIS\_TF.

$$\widetilde{\text{tfAmp}}_{bl\ c} = \frac{\widetilde{\text{visAmp}}_{bl\ c}}{J_1(\pi B_b/\lambda_l)/(\pi B_b/\lambda_l)} \quad (70)$$

$$\widetilde{\text{tfPhi}}_{bl\ c} = \widetilde{\text{visPhi}}_{bl\ c} \quad (71)$$



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### Interpolation of TF at the time of SCI

The TF are then averaged to obtain an estimation at the time of the SCI measurement:

$$\widetilde{\text{tfAmp}}_{bl} = \frac{\sum_c W_{bc} \widetilde{\text{visAmp}}_{blc}}{\sum_c W_{bc}} \quad (72)$$

where the weight is a combination of the distance in time  $(T - T_c)$ , and of the precision of the individual measurements:

$$W_{bc} = \frac{\exp(-2(T - T_c)^2/\Delta^2)}{\text{median}_l(\sigma_{blc}^2)} \quad (73)$$

The free parameter  $\Delta$  corresponds to the expected stability of the instrumental + atmosphere responses. Calibrations recorded within this time interval are mostly averaged, calibrations separated by about this time interval are mostly interpolated, and calibrations far away from this time interval will be discarded (closed one becomes dominant).

A similar approach is used for the phases:

$$\widetilde{\text{tfPhi}}_{bl} = \arg\left(\sum_c W_{bc} \exp(i \widetilde{\text{visPhi}}_{blc})\right) \quad (74)$$

### Calibration

$$\widetilde{\text{visAmp}}_{bl} = \frac{\widetilde{\text{visAmp}}_{bl}}{\widetilde{\text{tfAmp}}_{bl}} \quad (75)$$

$$\widetilde{\text{visPhi}}_{bl} = \arg\left(\exp(i(\widetilde{\text{visPhi}}_{bl} - \widetilde{\text{tfPhi}}_{bl}))\right) \quad (76)$$

## 10.20 Processing of ACQ

### Pre-processing

The pre-processing re-interpolates the bad-pixels. For the pupil images, the background is computed from the median of the images and subtracted.

### Analysis of pupil images

The pupil scale, rotation and position is computed for each frame by adjusting a spot model (16 spot on the expected grid) to the image. the degree of freedom are: rotation angle of pupil (same for the four sub-appertures), scaling of pupil (same for the four sub-appertures), mean x and y of each sub-apperture, FWHM (same for all diodes), and flux (one per diode).

The mean displacement of the pupil is computed (mean of the four sub-apperture) as PUPIL\_X and PUPIL\_Y. Then the expected opd introduced by the mean pupil displacement is computed by:

$$\text{OPD\_PUPIL} = \text{PUPIL\_S} \cdot \text{SEP} \cdot (\text{PUPIL\_X} \cos \Psi + \text{PUPIL\_Y} \sin \Psi) \quad (77)$$

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where  $\Psi$  is the angle of the binary separation in the ACQ camera frame, PUPIL\_S is the pupil scale (mm/pix) in the ACQ images (read from header, DROTOFF position), and SEP is the binary separation in [rad] (read from header).

## Analysis of field images

The positions on the acquisition camera detector of the SC and FT targets are measured by fitting a gaussian profile, after an initial guess based on the separation SOBJ.[X|Y], given in the main header, between the FT and SC targets. The results of the fitting process is available in table OI\_VIS\_ACQ, columns FIELD\_SC\_[X|Y] and FIELD\_FT\_[X|Y], with associated errors FIELD\_SC\_[X|Y]ERR and FIELD\_FT\_[X|Y]ERR.

In true dual-field mode, and when the separation SOBJ.[X|Y] is not zero, the plate scale of the acquisition camera is measured for each frame as the ratio between the separation and the distance between the two detected objects:

$$\text{FIELD\_SCALE} = \frac{||\text{SOBJ.}[X|Y]||}{||\text{FIELD\_SC\_}[X|Y] - \text{FIELD\_FT\_}[X|Y]||}, \quad (78)$$

and associated error FIELD\_SCALEERR.

In addition, an error signal FIELD\_FIBER\_D[X|Y] is generated between the detected SC/FT target relative positions and the SC/FT fibre relative positions, taking into account any dithering offset SOBJ.OFF[X|Y].

$$\begin{aligned} \text{FIELD\_D}[X|Y] = & (\text{FIELD\_SC}[X|Y] - \text{FIELD\_FT}[X|Y]) \\ & + \text{SOBJ.OFF}[X|Y]/\text{FIELD\_SCALE} \\ & - (\text{ACQ.FIBER.SC}[X|Y] - \text{ACQ.FIBER.FT}[X|Y]) \end{aligned} \quad (79)$$

This quantity is later used to unwrap the telescope metrology diode signals.

Finally, a Strehl ratio is estimated from each frame and stored in the FIELD\_STREHL column.

## 10.21 Processing of MET and FDDL

### From Volts to real time SC-FT phases

The signals of all diodes are analysed independently, without prior correction of the voltage, and converted into a real-time SC-FT phase for each diode. This real-time SC-FT phase is unwrapped and forced to match the OCS.MET reference. Both the unwrapping and the absolute reference are done with fringe-integer corrections only. These quantities are labeled OPD\_TEL and OPD\_FC in the OI\_VIS\_MET table.

### Averaging SC-FT phase inside SC DIT

The phase of a diode is averaged inside each SC DIT, as a scalar quantity (not phasor). This averaged signal is stored for each beam in OI\_FLUX table and each base in OI\_VIS table. These quantities are labeled OPD\_MET\_TEL and OPD\_MET\_FC.

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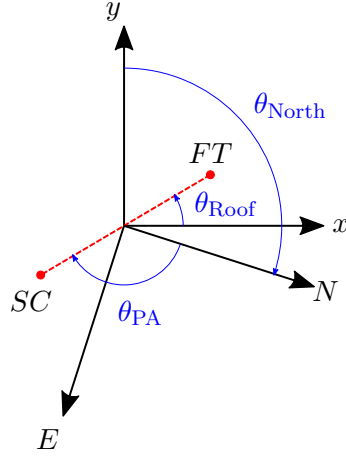


Figure 10.2: Geometry of the Acquisition Camera field image. The nominal positions of the *FT* and *SC* targets (red dots) are given in the acquisition camera field coordinates  $(x, y)$ . The orientation of the *FT/SC* pair matches the orientation of the roof prism  $\theta_{\text{Roof}}$  given by the keywords ESO.INS.DROTOFF $n$ . The direction of North  $\theta_{\text{North}}$  on the acquisition camera field is related to the position angle of the pair  $\theta_{\text{PA}}$ , calculated from the offset keywords ESO.INS.SOBJ.[X|Y], and to the roof angle  $\theta_{\text{Roof}}$ .

### Average the FDDL inside SC DIT

The mean SC and FT FDDLs strain gauge voltage during each frame of the SC, and per beam, is stored in the OI\_FLUX table. Columns are labelled SC\_POS and FT\_POS.

## 10.22 Applying dispersion correction to MET

### Correction of FFDL non linearity

The DISP\_MODEL provides, for each beam  $t$ :

- $\text{linSC}_{tm}$  : the non-linearity coefficients of order  $m$  of the SC FDDL.
- $\text{linFT}_{tm}$  : the non-linearity coefficients of order  $m$  of the FT FDDL.

SC\_POS and FT\_POS are first corrected from non-linearity of the strain gauge, and then averaged to get the mean position of the two fibers:

$$\text{FDDL}_{tf} = \frac{\sum_m (\text{linSC}_{tm} \text{SC\_POS}_{tf}^m) + \sum_m (\text{linFT}_{tm} \text{FT\_POS}_{tf}^m)}{2} \quad (80)$$

### Dispersion-included metrology signal

The DISP\_MODEL allows to compute the *mean* refractive index of SC and FT FDDL at wavelength  $l$  for each beam  $t$ , normalized to the one at the metrology wavelength (hereafter called  $n_{\text{mean}_{tl}}$ ); and the *differential*

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refractive index between SC and FT FDDL wavelength  $l$  for each beam  $t$ , normalized to the one at the metrology wavelength (hereafter called  $\text{ndiff}_{tl}$ ).

In practice, these two quantities are stored as a polynomial model versus wavenumber, centered in the middle of the K-band ( $\lambda_0 = 2.2\mu\text{m}$ ):

$$\text{nmean}_{tl} = \sum_m \left( \text{nmean}_{tm} \left( \frac{\lambda_0}{\lambda_l} - 1 \right)^m \right) \quad (81)$$

$$\text{ndiff}_{tl} = \sum_m \left( \text{ndiff}_{tm} \left( \frac{\lambda_0}{\lambda_l} - 1 \right)^m \right) \quad (82)$$

where  $\text{nmean}_{tm}$  and  $\text{ndiff}_{tm}$  are the polynomial coefficients of order  $m$  of beam  $t$ , read from the DISP\_MODEL.

From the dispersion and the metrology signal, we can compute the amount of delay introduced by the differential delay-line, for each spectral channel and each baseline. This quantity is called  $\text{OPD\_DISP}_{bfl}$ :

$$\begin{aligned} \text{OPD\_DISP}_{bfl} = & \text{nmean}_{t_1 l} \text{OPD\_MET\_FC}_{t_1 f} - \text{nmean}_{t_2 l} \text{OPD\_MET\_FC}_{t_2 f} + \\ & \text{ndiff}_{t_1 l} \text{FDDL}_{t_1 f} - \text{ndiff}_{t_2 l} \text{FDDL}_{t_2 f} \end{aligned} \quad (83)$$

### Dispersive group-delay and remaining phase

The signal  $\text{OPD\_DISP}_{bfl}$  contains a fraction of group-delay coded as a spectral slope. This shall be properly taken into account when attempting to compute astrometric/absolute phases out of the dataset.

Therefore the pipeline also provide an additional representation of the same quantity, but decomposed into the total group-delay in the middle of the K-band ( $\text{GDELAY\_DISP}_{bf}$  in unit of distance, thus [m]), and the remaining phase ( $\text{PHASE\_DISP}_{lbf}$ , in [rad]).

The total group-delay introduced by FDDL in the middle of the band is:

$$\text{GDELAY\_DISP}_{bf} = \frac{\lambda_{l_1}^{-1} \text{OPD\_DISP}_{l_1 bf} - \lambda_{l_2}^{-1} \text{OPD\_DISP}_{l_2 bf}}{\lambda_{l_1}^{-1} - \lambda_{l_2}^{-1}} \quad (84)$$

where  $l_1$  and  $l_2$  are two consecutive wavelength channel in the middle of the band. The remaining phase is:

$$\text{PHASE\_DISP}_{lbf} = \arctan \left( \exp \left( \frac{2i\pi}{\lambda_f} (\text{OPD\_DISP}_{lbf} - \text{GDELAY\_DISP}_{bf}) \right) \right) \quad (85)$$

The  $\text{GDELAY\_DISP}_{bf}$  quantities are defined to within a constant: the so-called dispersed metrology zeros  $\text{Z\_DISP}_t$  (one per beam). When combined with the group-delays from SC and FT, the  $\text{GDELAY\_DISP}_{bf}$  can be used to construct a group-delay astrometry, e.g:

$$\begin{aligned} \vec{B}_{b_{ij}} \cdot \vec{\delta} + (\text{Z\_DISP}_i - \text{Z\_DISP}_j) = & \text{GDELAY\_DISP}_{b_{ij}f} \\ & - (\text{GDELAY\_SC}_{b_{ij}f} - \text{GDELAY\_FT}_{b_{ij}f}) \end{aligned} \quad (86)$$

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In order to use the telescope metrologies, additional corrections need to be added to the astrometric equation above:

$$\begin{aligned}
\vec{B}_{bij} \cdot \vec{\delta} + (Z\_DISP_i - Z\_DISP_j) = & \text{GDELAY\_DISP}_{bijf} \\
& + (\text{TELFC\_MCORR} + \text{FC\_CORR}) \\
& - (\text{GDELAY\_SC}_{bijf} - \text{GDELAY\_FT}_{bijf})
\end{aligned} \quad (87)$$

### 10.23 Astrometric transformations and projected baseline

Due to its astrometric requirements, the pipeline uses the ERFA astrometric library (derived from SOFA) to transform coordinates between the Celestial and Observed reference frames. The SOFA documentation gives a good description of the transformations between the two reference frames; the present manual only describes its use.

For each observation, the mid-point  $(\alpha_c, \delta_c)$  between the FT and SC targets in celestial (ICRS) is first converted into barycentric (BCRS) by applying space motion (proper motion, parallax, and radial velocity).

$$(\alpha_c, \delta_c) \Rightarrow (\alpha_b, \delta_b) \equiv \vec{e}_{Wb} \quad (88)$$

The equatorial directions  $(\vec{e}_{Ub}, \vec{e}_{Vb})$  are then computed from the pointing direction  $\vec{e}_{Wb}$  and the direction of the pole  $\vec{e}_{Zb}$  as follows:

$$\vec{e}_{Ub} = \frac{\vec{e}_{Zb} \times \vec{e}_{Wb}}{\|\vec{e}_{Zb} \times \vec{e}_{Wb}\|} \quad (89)$$

$$\vec{e}_{Vb} = \vec{e}_{Wb} \times \vec{e}_{Ub} \quad (90)$$

The unit vectors  $\vec{e}_{Ub}$  and  $\vec{e}_{Vb}$  point in the direction of increasing right ascension and declination respectively.

Since ERFA is only capable of transforming coordinates, a set of four coordinates at a small  $\epsilon = \pm 10 \text{ arcsec}$  angle in right ascension and declination is used instead: the cardinal asterism. They are created by rotating the pointing direction  $\vec{e}_{Wb}$  around the right ascension and declination directions  $(\vec{e}_{Ub}, \vec{e}_{Vb})$  by this small  $\epsilon$  angle.

$$(\alpha_b + \epsilon, \delta_b) \equiv \vec{e}_{W+Ub} = \mathcal{R}_{-\epsilon \vec{e}_{Vb}}(\vec{e}_{Wb}) \quad (91)$$

$$(\alpha_b - \epsilon, \delta_b) \equiv \vec{e}_{W-Ub} = \mathcal{R}_{+\epsilon \vec{e}_{Vb}}(\vec{e}_{Wb}) \quad (92)$$

$$(\alpha_b, \delta_b + \epsilon) \equiv \vec{e}_{W+Vb} = \mathcal{R}_{+\epsilon \vec{e}_{Ub}}(\vec{e}_{Wb}) \quad (93)$$

$$(\alpha_b, \delta_b - \epsilon) \equiv \vec{e}_{W-Vb} = \mathcal{R}_{-\epsilon \vec{e}_{Ub}}(\vec{e}_{Wb}) \quad (94)$$

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ERFA is then used to transform the pointing origin and cardinal asterism coordinates from barycentric to observed reference frame. This transformation uses the Earth Orientation Parameters (UT1-UTC and polar motion) published by the IERS.

$$(\alpha_b, \delta_b) \Rightarrow (\alpha_o, \delta_o) \equiv \vec{e}_{Wo} \quad (95)$$

$$(\alpha_b + \epsilon, \delta_b) \Rightarrow (\alpha_o + \epsilon, \delta_o) \equiv \vec{e}_{W+Uo} \quad (96)$$

$$(\alpha_b - \epsilon, \delta_b) \Rightarrow (\alpha_o - \epsilon, \delta_o) \equiv \vec{e}_{W-Uo} \quad (97)$$

$$(\alpha_b, \delta_b + \epsilon) \Rightarrow (\alpha_o, \delta_o + \epsilon) \equiv \vec{e}_{W+Vo} \quad (98)$$

$$(\alpha_b, \delta_b - \epsilon) \Rightarrow (\alpha_o, \delta_o - \epsilon) \equiv \vec{e}_{W-Vo} \quad (99)$$

Then the pointing directions to the cardinal asterism are combined to generate the equatorial directions  $(\vec{e}_{Uo}, \vec{e}_{Vo})$  in the observed reference frame.

$$\vec{e}_{Uo} = \frac{1}{2\epsilon} \vec{e}_{Wo} \times (\vec{e}_{W+Uo} \times \vec{e}_{W-Uo}) \quad (100)$$

$$\vec{e}_{Vo} = \frac{1}{2\epsilon} \vec{e}_{Wo} \times (\vec{e}_{W+Vo} \times \vec{e}_{W-Vo}) \quad (101)$$

Even though  $(\vec{e}_{Ub}, \vec{e}_{Vb}, \vec{e}_{Wb})$  is an orthonormal basis in the barycentric reference frame,  $(\vec{e}_{Uo}, \vec{e}_{Vo}, \vec{e}_{Wo})$  is not orthonormal in the observed reference frame. The pointing vector  $\vec{e}_{Wo}$  is a unit vector, but the right ascension and declination vectors  $(\vec{e}_{Vo}, \vec{e}_{Wo})$  are not: they carry a scaling factor associated to the effect of astronomical aberration.

The azimuth and zenith distance directions  $(\vec{e}_{AZo}, \vec{e}_{ZDo})$  are also calculated from the observed pointing direction  $\vec{e}_{Wo}$  and the zenith direction  $\vec{e}_{Zo}$ .

$$\vec{e}_{AZo} = \frac{\vec{e}_{Wo} \times \vec{e}_{Zo}}{\|\vec{e}_{Wo} \times \vec{e}_{Zo}\|} \quad (102)$$

$$\vec{e}_{ZDo} = \vec{e}_{Wo} \times \vec{e}_{AZo} \quad (103)$$

The vectors  $\vec{e}_{Uo}, \vec{e}_{Vo}, \vec{e}_{Wo}, \vec{e}_{AZo}, \vec{e}_{ZDo}$  populate the columns **E\_U**, **E\_V**, **E\_W**, **E\_AZ**, **E\_ZD** of the pipeline products.

Finally, the projected baseline is calculated as the scalar product between the physical baseline  $\vec{B}_o$  in the observed reference frame and the equatorial directions  $(\vec{e}_{Uo}, \vec{e}_{Vo})$  also in the observed reference frame.

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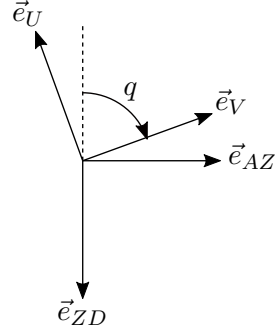


Figure 10.3: Geometry in the pupil, looking toward the target. It shows the azimuth and zenith distance directions ( $\vec{e}_{AZ}, \vec{e}_{ZD}$ ), the right ascension and declination directions ( $\vec{e}_U, \vec{e}_V$ ), and the parallactic angle  $q$ .

$$B_{Ub} = \vec{B}_o \cdot \vec{e}_{Uo} \quad (104)$$

$$B_{Vb} = \vec{B}_o \cdot \vec{e}_{Vo} \quad (105)$$

The projections  $B_{Ub}, B_{Vb}$  populate the columns **UCOORD**, **VCOORD** of the pipeline products.

Last element of importance, the baseline vector  $\vec{B}_o$  in the observed reference frame is supposed to be the physical or vacuum vector. However, the telescope positions reported in the fits headers correspond to OPD models that are scaled by the refractive index of air ( $n = 1.0002028$ ) at the atmospheric pressure of Paranal and at the wavelength of the Helium Neon laser of the VLT delay lines. The pipeline takes care of compensating this refractive index scaling when computing the observed baseline from the headers.

$$\vec{B}_o = 1/n \vec{B}_{header} \quad (106)$$

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## A Installation

One is advised to read the installation instructions delivered with the GRAVITY pipeline distribution kit. These release-specific instructions can be found in the file `README` located in the top-level directory of the unpacked GRAVITY pipeline source tree. The supported platforms are listed in Section A.1. It is recommended reading through Section A.2.2 before starting the installation.

A bundled version of the GRAVITY pipeline with all the required tools and an installer script is available from <http://www.eso.org/pipelines/>, for users who are not familiar with the installation of software packages.

### A.1 Supported platforms

The utilisation of the GNU build tools should allow to build and install the GRAVITY pipeline on a variety of UNIX platforms, but it has only been verified on the VLT target platforms:

- Linux (glibc 2.1 or later),
- Sun Solaris 2.8 or later,

using the GNU C compiler (version 3.2 or newer).

### A.2 Building the GRAVITY pipeline

This section shows how to obtain, build and install the GRAVITY pipeline from the official source distribution.

#### A.2.1 Requirements

To compile and install the GRAVITY pipeline one needs:

- the GNU C compiler (version 3.2 or later),
- the GNU `gzip` data compression program,
- a version of the `tar` file-archiving program, and,
- the GNU `make` utility.

An installation of the Common Pipeline library (CPL) must also be available on the system. Currently the CPL version 2.1.1 or newer is required. The CPL distribution can be obtained from [3].

Please note that CPL itself depends on an existing `qfits` installation. The `qfits` sources are available from the CPL download page or directly from the `qfits` homepage at <http://www.eso.org/projects/aot/qfits>. In conjunction with CPL 2.1.1 `qfits` 5.3.1 must be used.



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In order to run the GRAVITY pipeline recipes a front-end application is also required. Currently there are two such applications available, a command-line tool called *EsoRex* and the Java based data file organizer, *Gasgano*, which provides an intuitive graphical user interface (see Section 5.2, page 17). At least one of them must be installed. The *EsoRex* and *Gasgano* packages are available at <http://www.eso.org/cpl/esorex.html> and <http://www.eso.org/gasgano> respectively.

For installation instructions of any of the additional packages mentioned before please refer to the documentation of these packages.

## A.2.2 Compiling and installing the GRAVITY pipeline

The GRAVITY pipeline distribution kit 1.0 contains:

gravity-manual-1.0.pdf	The GRAVITY pipeline manual
install_pipeline	Install script
cpl-7.1.tar.gz	CPL 7.1
esorex-3.13.tar.gz	esorex 3.13
gasgano-2.4.8.tar.gz	GASGANO 2.4.8for Linux
gravity-1.2.1.tar.gz	GRAVITY 1.2.1
gravity-calib-1.2.1.tar.gz	GRAVITY calibration files 1.2.1

Here is a description of the installation procedure:

1. Change directory to where you want to retrieve the GRAVITY pipeline recipes 1.2.1package. It can be any directory of your choice but not:

```
$HOME/gasgano
$HOME/.esorex
```

2. Download from the ESO ftp server, <http://www.eso.org/pipelines/>, the latest release of the GRAVITY pipeline distribution.
3. Verify the checksum value of the tar file with the cksum command.
4. Unpack using the following command:

```
tar -xvf \pipename-kit-\pipelinevers.tar
```

Note that the size of the installed software (including *Gasgano*) together with the static calibration data is about 1.3 Gb, mainly du to the test data.

5. Install: after moving to the top installation directory,

```
cd \pipename-kit-\pipelinevers
```

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it is possible to perform a simple installation using the available installer script (*recommended*):

```
./install_pipeline
```

(beware: the execution may take a few minutes on Linux and several minutes on SunOS).

Note that this release still needs to link to the eclipse library. At the end of the installation the user in addition to follow what reported by the installation script, needs to source an file (\$HOME/..eclipse\_bash.rc or \$HOME/..eclipse\_bash.rc, depending from the user shell) to set a few environment variables used by a few low level eclipse library based modules.

By default the script will install the GRAVITY recipes, *Gasgano*, *EsoRex*, all the necessary libraries, and the static calibration tables, into a directory tree rooted at \$HOME. A different path may be specified as soon as the script is run.

The only exception to all this is the *Gasgano* tool, that will always be installed under the directory \$HOME/gasgano. Note that the installer will move an existing \$HOME/gasgano directory to \$HOME/gasgano.old before the new *Gasgano* version is installed.

Important: the installation script would ensure that any existing *Gasgano* and *EsoRex* setup would be inherited into the newly installed configuration files (avoiding in this way any conflict with other installed instrument pipelines).

Alternatively, it is possible to perform a manual installation (*experienced users only*): the README file located in the top installation directory contains more detailed information about a step-by-step installation.

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## B Abbreviations and acronyms

ANSI	American National Standards Institute
ASCII	American Standard Code for Information Interchange
CalibDB	Calibration Database
CPL	Common Pipeline Library
DFO	Data Flow Operations department
DFS	Data Flow System department
DHS	Data Handling Server
DO	Data Organizer
DMD	Data Management and Operations Division
DRS	Data Reduction System
ESO	European Southern Observatory
ESOREX	ESO-Recipe Execution tool
FDDL	Fibered Differential Delay Lines
FITS	Flexible Image Transport System
FOV	Field Of View
FT	Fringe-Tracker
SC	Science-Combiner
GUI	Graphical User Interface
OB	Observation Block
OIFITS	OIFITS format, see [4]
PSO	Paranal Science Operations
QC	Quality Control
RON	Read Out Noise
SOF	Set Of Frames
UT	Unit Telescope
AT	Auxiliary Telescope
VLTI	Very Large Telescope Interferometer